



## Heat transfer — a review of 1996 literature

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## 1. Introduction

The present review is designed to encompass the English language heat transfer papers published in 1996. The papers have been categorized into a number of sub-fields. While being exhaustive, some selection is necessary. Besides reviewing the journal articles of 1996, we also briefly mention important conferences and meetings on heat transfer and related fields, major awards and also books on heat transfer published during the year.

A Meeting on Molecular and Microscale Heat

Transfer in Materials Processing and Other Applications was held in Yokohama, Japan on February 2–7. Topics covered included the following: molecular dynamics approach to heat conduction, microscale heat transfer in thin film formation and plasma processing, and measurement of temperature and thermophysical properties using atomic and molecular scale phenomena. The Turbulent Heat Transfer Conference was held on March 10–15 in San Diego, USA. The 3rd International Heat and Mass Transfer Forum was organized in Minsk, Belarus on May 20–24. The 2nd European Thermal-Sciences and 14th Italian Union of

Thermo-Fluid-Dynamics (UIT) National Heat Transfer Conference was held on May 29–31 in Rome, Italy; sessions were held on experimental work and a variety of new experimental techniques. The 41st Gas Turbine and Aeroengine Congress, User's Symposium and Exhibition "ASME Turbo Expo'96-Land, Sea and Air" was organized by ASME International in Birmingham, England on June 10–13. Topics covered, among others, were film cooling of gas turbine blades, internal heat transfer, including the effects of rib roughness, rotation and secondary flows, and external heat transfer to blades. The 31st AIAA Thermophysics Conference held on June 18–20 in New Orleans, USA had sessions on surface catalysis, ablation, direct simulation, Monte Carlo methods and nonintrusive diagnostics. A Meeting on Advanced Computational Methods in Heat Transfer was held on July 8–10 in Udine, Italy. Subjects of discussion included convection–diffusion problems, fire and combustion simulation, computational aspects of thermal problems in porous media, metal casting and forging and combined heat and mass transfer. The 31st National Heat Transfer Conference was held in Houston, USA on August 3–6. The proceedings each day consisted of technical sessions, keynote lectures and short courses. Of particular interest were the sessions on extending air cooling limits for thermal management of electronics, interfacial phenomena and thermophysics in microgravity, combustion and fire, solution methods for radiative heat transfer in participating media and thermal management of commercial and military electronics.

The International Symposium on Transient Convective Heat Transfer organized by the International Centre for Heat and Mass Transfer (ICHMT) in Cesme, Turkey on August 19–23 included papers on boundary layers, internal forced convection, mixed and free convection, heat exchangers and thermal equipment and conjugate heat transfer. At the 14th European Conference on Thermophysical Properties on September 16–19 in Villeurbanne, France, sessions covered measurement methods for thermal conductivity, diffusivity and effusivity, optical and radiative properties, permeability, phase equilibrium and surface tension for a wide range of materials including metals and alloys, ceramics, polymers and composites, superconductors and insulators. At the 4th International Symposium on Heat Transfer on October 7–11 in Beijing, China, among topics covered were micro heat transfer in space and time, multiphase flow and heat transfer, heat and mass transfer in porous media and biological and cryogenic heat transfer.

At the International Mechanical Engineering Congress and Exposition (formerly known as the Winter Annual Meeting of the ASME) held on November 17–22 in Atlanta, USA, technical sessions covered exper-

imental studies in multiphase flow, turbulent heat transfer, heat transfer in microgravity systems, jets and sprays, and cryogenic heat transfer in the energy industry. The International Conference on Heat Transfer with Change of Phase "HEAT '96" was held in Kielce, Poland on December 8–10. Topics covered included pool boiling, condensation, melting and solidification and sublimation. The sixth Australasian Heat and Mass Transfer Conference held on December 9–12 at the University of New South Wales, Sydney, Australia included sessions held on contact conductance, heat transfer in fires, heat and mass transfer in drying, experimental methods and environmental heat and mass transfer.

Awards presented in 1996 included the (1995) Max Jakob Award to Professor Arthur E. Bergles for his outstanding contributions in the areas of enhanced heat transfer, two-phase flow and boiling heat transfer and internal laminar flows, the (1995) Donald Q. Kern Award of the AIChE to Dr. George Bankoff and the 1996 Heat Transfer Memorial Awards to Professor Boris Rubinsky (Art of Heat Transfer), Professor Ping Cheng (Science) and Professor Leroy 'Skip' Fletcher (General). The Luikov Award instituted by the ICHMT was given to Dr. Geoffrey Hewitt.

Several books on heat transfer, related to both fundamentals and applications, were published during the year:

Advanced Computational Methods in Heat Transfer IV

L. C. Wrobel, C. A. Brebbia, A. J. Nowak  
Publisher: Computational Mechanics

Advances in Heat Transfer : Transport Phenomena in Materials Processing (Vol. 28)

James P. Hartnett

Publisher: Academic Press

Advances in Numerical Heat Transfer, Vol. 1

W. J. Minkowycz, E. M. Sparrow (Eds.)

Publisher: Hemisphere

Chemical Engineering : Fluid Flow, Heat Transfer and Mass Transfer Vol. 1 (5th ed.)

J. M. Coulson, J. F. Richardson, J. R. Blackhurst and J. H. Harker

Publisher: Butterworth–Heinemann

Computational Heat Transfer Vol. 1

A. A. Samarskii, P. N. Vabishchevich

Publisher: Wiley

Computational Heat Transfer: The Finite Difference Methodology Vol. 2

A. A. Samarskii, P. N. Vabishchevich

Publisher: Wiley

Convective Flow Boiling: Proceedings of Convective Flow Boiling, an International Conference Held at the Banff Center for Conferences, Banff, Alberta

John C. Chen (Ed.), Yasunobu Fujita, Franz Mayinger

Publisher: Taylor & Francis  
 The Finite Element Method in Heat Transfer Analysis  
 R. W. Lewis, K. Morgan (Eds.)  
 Publisher: Wiley  
 The Finite Element Method in Heat Transfer Analysis  
 R. W. Lewis (Ed.)  
 Publisher: Wiley  
 Flow and Heat Transfer in Rotating-Disc Systems: Rotating Cavities (Vol. 2)  
 J. M. Owen, R. H. Rogers  
 Publisher: Wiley  
 Fundamentals of Heat and Mass Transfer (4th ed.) and Interactive Heat Transfer Set  
 David P. DeWitt, Frank P. Incropera  
 Publisher: Wiley  
 Gas-Turbine Regenerators  
 Douglas Stephen Beck, David Gordon Wilson and Douglass Beck  
 Publisher: Chapman & Hall  
 Heat and Mass Transfer in Severe Nuclear Reactor Accidents  
 J. T. Rogers (Ed.)  
 Publisher: Begell House  
 Heat Transfer  
 C. Suryanarayana  
 Publisher: PWS  
 Heat Transfer: A Self-Instructional Problem Workbook  
 Joseph P. Reynolds, Ihab H. Farag  
 Publisher: ETS  
 Heat Transfer in Condensation  
 R. Vidil (Ed.)  
 Publisher: Elsevier  
 Heat Transfer Technologies and Practices For Effective Energy Management  
 G. Sam Samdani (Ed.)  
 Publisher: McGraw-Hill  
 Heat and Mass Transfer Under Plasma Conditions: Proceedings of International Symposium on Heat and Mass Transfer Under Plasma Conditions  
 Publisher: Begell House  
 Introduction to Heat Transfer (3rd ed.) and Interactive Heat Transfer Set  
 David P. DeWitt, Frank P. Incropera  
 Publisher: Wiley  
 Introduction to Thermodynamics and Heat Transfer (McGraw-Hill Series in Mechanical Engineering)  
 Yunus A. Cengel  
 Publisher: McGraw-Hill  
 Latent Heat Transfer: An Introduction to Fundamentals (Oxford Engineering Science Series, No. 43)  
 G. S. H. Lock  
 Publisher: Oxford University Press  
 Macro-To Microscale Heat Transfer: The Lagging

Behavior (Series in Chemical and Mechanical Engineering)

D. Y. Tzou  
 Publisher: Taylor & Francis  
 Principles of Heat Transfer (5th ed.)  
 Frank Kreith, Mark S. Bohn  
 Publisher: PWS  
 Principles of Heat Transfer in Porous Media (2nd ed.)  
 M. Kaviany  
 Publisher: Springer-Verlag  
 Process, Enhanced, and Multiphase Heat Transfer: A Festschrift for A.E. Bergles  
 A. E. Bergles (Ed.)  
 Publisher: Begell House  
 Radiation Heat Transfer in Disperse Systems  
 L. A. Dombrovsky  
 Publisher: Begell House  
 Radiative Heat Transfer I: Proceedings of the First International Symposium on Radiation Transfer, Kusadasi, Turkiye, August 13–18, 1995  
 M. Pinar Menguc (Ed.)  
 Publisher: Begell House  
 Transport Phenomena in Materials Processing  
 Sindo Kou  
 Publisher: Wiley  
 Two-Phase Flow and Heat Transfer (Oxford Chemistry Primers, 42)  
 P. B. Whalley  
 Publisher: Oxford University Press

## 2. Conduction

Various papers encompassing Conduction Heat Transfer are reviewed in this section. The relevant papers are subcategorized into the following topics: contact conduction/contact resistance; layered, composite or heterogeneous media and other effects; thermal waves, laser and pulse heating effects and/or applications; heat conduction in fins, tubes, solids and different geometries; mathematical models, analytic/numerical, and experimental studies; thermo-mechanical issues; inverse problems; conduction–convection and flow effects; solidification and change of phase, micro-electronic heat transfer; materials processing and process modeling; specialized and miscellaneous studies and applications.

### 2.1. Contact conduction/contact resistance

The papers in this subcategory deal with errors in the analysis of a lumped parameter assumption and heat flow in surfaces which accounts for thermal contact resistance [1A]; issues involving thermal contact

conductance in diamond-like films and refractory ceramic coatings [2A,3A]; a closed form solution of junction to substrate thermal resistance in semi-conductor chips [4A]; and models for elastoplastic contact conductance for isotropic conforming rough surfaces and contact conductance of tool steel [5A,6A]. The effects of interface resistance on the heat transfer in cold rolling of steel appears by [7A].

## 2.2. Composite and heterogeneous media

Issues encompassing effective thermal conductivity in composite media are addressed in [8A,9A,11A,12A,17A]. Other papers dealing with thermal aspects in this subcategory include: a model for in-situ tow placement of thermoplastic composites [10A], issues regarding the thermoelastic field in composites with inhomogeneities [13A], design of a tungsten/copper graded composite for high heat flux components [14A], optimization of multi-layer high temperature insulation [18A], thermal stress analysis and pultrusion of epoxy matrix composites [15A,16A], and interface properties of nanocomposites employing nonlinear optics [19A].

## 2.3. Thermal waves, laser and pulse heating applications

A paper on laser annealing of silicon appears by [20A], [21A] and [22A] discuss hyperbolic propagation of thermal phenomenon in an infinite solid medium and a cylindrical solid carrying a steady-periodic electric field, respectively. Recent progress in laser surface treatment as pertaining to laser wavelength issues appear in [23A]. [24A,25A] discuss thermal inertia of materials and velocity of thermal waves generated by femtosecond laser pulses in thick gold films, respectively. [26A–31A] describe analytic solutions and issues for a variety of situations for problems influenced by non-Fourier heat conduction. The so-termed first and second-law efficiencies for laser drilling of stainless steel appears by [32A], and [33A] describes heat conduction in a semi-infinite solid due to a time-dependent laser source.

## 2.4. Heat conduction in fins, tubes, solids and different geometries

[34A] describe optimum design of radiating and convective-radiating fins, and the study of heat removal from tubes with external longitudinal fins appears by [35A]. Other related studies involving fin/tube geometries and solids appear in [36A–53A].

## 2.5. Mathematical models, simulations and/or experimental results

Numerous papers appear in this category dealing with closed form solutions, analytic approximation, numerical simulations and experimental studies on a variety of applications including heat conduction. Those dealing with providing analytic/approximate solutions appear due to [54A], [67A], [73A], [78A], and [79A]. Those dealing with numerical simulations and applications involving control volume methods, finite element, boundary element and the like appear for different applications in [55A–66A,68A–72A,74A–77A,80A,81A,83A–91A,94A–100A]. Other related experimental and/or comparative studies appear due to [82A], [92A], and [93A].

## 2.6. Thermo-elastic and thermo-mechanical problems

[101A] describes a thermoelasto-hydrodynamic analysis of fixed geometry thrust bearings. The interaction of a crack and a circular elastic inclusion under uniform heat flow appears by [102A]. A numerical investigation of a finite multi-grid solver for thermo-elastic stress analysis in anisotropic materials appears [103A] and that of three-dimensional thermoelastic contact between two plates with bolted joints appears by [104A]. [108A] discuss Biot's number and thermal stress fields in liquid quenches for ceramics. [109A] discuss thermo-mechanical issues during diffusion bonding of metal drum rotor disks under electromagnetic heating. Other relevant papers involving thermal stresses for an infinite plate containing a penny-shaped crack, thermally induced bending vibrations, axisymmetric thermal stresses in steady state and in transient behavior in composite brake disks, in functionally graded materials, and control of deformation in laminated plates and appears due to [105A–107A,110A–112A].

## 2.7. Inverse problems and applications

The comparison of some inverse heat conduction methods using experimental data appears by [113A]. A semi-numerical method for solving inverse heat conduction problems is studied by [114A] and [115A] discusses a second-order finite difference approximation for inversely determining thermal conductivity.

## 2.8. Flow/convection effects and change of phase

The papers appearing in this subcategory deal with the influence of flow and/or convection effects on heat conduction with and/or without considerations involving change of phase. [117A] describe a modified effective capacitance method for solidification modeling.

[118A,119A] study heat transfer effects in spheres and [120A] discuss heat transfer between a spherical droplet particle and a two-phase fluid. An investigation of the relations between the results in heat conduction problems appears by [121A]. Other related studies involving heat transfer influenced by convective heat transfer appear due to [116A,122A–131A].

### 2.9. Microelectronic heat transfer

In this subcategory, [132A] investigated thermal modeling in integrated power circuits; [133A] describes thermal conduction in nonhomogeneous CVD diamond layers in electronic microstructures; [134A] conduct a comparison of the cooling performance of staggered and in-line arrays of a polymer insulator; [135A] describe electrical and thermal performance of a polymer insulator; and [136A] conduct a study on board and system level effects on plastic package thermal performance.

### 2.10. Miscellaneous studies and special applications

A variety of specialized applications and other miscellaneous studies also appear in the heat conduction category. These are identified in papers [137A–171A].

## 3. Boundary layers and external flows

The papers on boundary layers and external flows for 1996 have been categorized as follows: flow influenced externally, flows with special geometric effects, compressible and high-speed flows, analysis and modeling techniques, unsteady flow effects, flows with film and interfacial effects, flows with special fluid types and property effects, and flows with combustion or reaction.

### 3.1. External effects

Papers which focus on external effects document the influence of elevated freestream turbulence on heat transfer [9B,7B] or of the unsteadiness due to the presence of an adjacent rod [8B,3B] or a vibrating wall surface [6B]. One with an elevated freestream turbulence was also strongly thermally stratified [4B]. Another paper in this category investigated the effects of extra rates of strain on turbulent transport [5B] while one noted the gravitational effect on heat transfer from horizontal surfaces [1B]. The final paper in this category [2B] determined the current density limit within electrodeposition cells.

### 3.2. Geometric effects

Several papers focused on geometrical effects on heat transfer in the stagnation region of a blunt object [16B,12B,17B,14B]. Several were on the heat transfer from cylinders in cross flow [10B,21B,26B,27B,13B,15B]. One [13B] extended this study to include spheres and another [15B] investigated tubular reactor geometries. One study documented heat transfer in the endwall-boundary layer region downstream of a streamlined strut [25B] while another computed the flow transition over a turbine airfoil [28B]. There were several papers which documented the improvement in heat transfer one can find with augmentation devices; one spoke of augmentation in general [11B], one investigated a chevron-type heat exchanger surface [20B] while several looked at trenches, dimples and protuberances [24B,18B]. Rather special geometries were, asymmetric-ribbed surfaces [19B], a damper of a water heater [22B], and a stretching sheet [23B].

### 3.3. Compressibility and high-speed flow effects

The most common subtopic of papers on compressibility investigated shock-boundary layer interaction effects. Papers on this category included a review of the topic [39B], several on modeling [30B,38B,33B,41B], one on measurements [32B], one which documented the effects of upstream influences [36B], and another which focused on expansion corner effects [43B]. There were several fundamental studies on compressible flow effects which included one on electron and vibration kinetics [31B], another on boundary layer transition [35B], and another which presented a nonequilibrium algebraic model for turbulent density fluctuations [42B]. Two papers which were specific to a geometry included one with a blunt core [34B] and another with a transverse jet [37B]. One paper discussed the boundary layer with an impulsively-started wedge [29B] and another discussed hot-wire measurements in hypersonic flows [40B].

### 3.4. Analysis and modeling

There was considerable activity in the modeling category. Papers on model development included a review of papers on numerical heat transfer [59B], the introduction of a new dimensionless number for forced convection heat transfer [46B], a mechanistic model of heat transfer from a wall to a fluid [50B], an evaluation of temperature effects in laminar boundary layer stability [49B], molecular modeling of shear flow [57B], and modeling of the turbulent transport of heat [44B,60B,61B]. Modeling was tested against a retarded boundary layer [53B], general advection–diffusion



problems [58B], a planar Couette flow [48B], turbine cascade flows [45B], and electronic modules [52B]. Other applications included separated and impinging flows [51B], thermally stratified flows [56B,47B], thermally mixed flows [55B], and atmospheric boundary layers [54B].

### 3.5. Unsteady effects

Unsteadiness was the theme for papers which investigated an impulsively started plate [63B], a step in cooling [62B], oscillating flow [65B], and boundary layer transition [67B, 68B]. Application papers included a study of thermal flow sensor dynamics [66B], and others on the unsteadiness of a three-dimensional wake [64B] or the junction of a cylinder and a boundary layer [69B].

### 3.6. Films and interfacial effects

Flows in this category included several on falling films; one with a gravity-driven laminar film [75B], another with water and lithium bromide [72B], one with roll waves [74B], and one in a falling film reactor [71B]. Other geometries included a two-phase, gas–liquid flow [73B] and an evaporating spray [70B].

### 3.7. Effects of fluid type or fluid properties

In this category, the Colburn analogy was evaluated for nonNewtonian liquids [87B], and heat transfer boundary layer solutions were found for a power-law fluid [81B]. One analysis of a flat plate boundary layer was done for a micropolar fluid [82B] while another investigated experimentally a microfluid system [85B]. Two papers dealt with superfluid helium [84B,77B], one in a boundary layer and another in a channel. A Dittus–Boelter type expression for heat transfer in fluids at supercritical pressures was suggested which had a new method for finding the equivalent specific heat [80B] and expressions were presented for heat transfer in a rarefied gas [78B]. Two computational papers were presented for particle-laden flows [76B,86B], one recommended a particular treatment of the carrier gas and another presented a new technique for dealing with particle-induced disturbances. Finally, a study was applied to the mass transfer resistance in the pervaporation process [83B] and another specifically dealt with heat transfer in food products [79B].

### 3.8. Flows with combustion and reaction

Several papers in this category dealt with combustion processes, one showed heat loss effects on turbulent flame propagation [88B], another looked at heat

transfer in a reverse flow combustor [91B], a third [95B] discussed diffusion flames under microgravity conditions, another investigated combustion wave propagating through a heterogeneous powder mixture [94B], and one reviewed flame impingement heat transfer correlations for industrial heating and melting [89B]. Two papers dealt with condensation and deposition; one presented a hydrodynamic principle for CVD reactors which allow homogeneous deposition of layers [93B] and another shows measurements of convection flows in physical vapor deposition [92B]. A numerical model was presented for analyzing hot-spot formation and growth to detonation in condensed-phase energetic materials [90B].

## 4. Channel flows

Channel flows were divided into the following subcategories: straight-walled ducts; irregular geometries; finned and profiled ducts; ducts experiencing secondary motion; pulsatile or oscillatory flow; two-phase flow in ducts [also see separate section on two-phase flow]; nonNewtonian flow; and miscellaneous duct flows.

### 4.1. Straight-walled ducts

Heat transfer in straight-walled ducts continues to be an active area of research. General correlations for turbulent flow and heat transfer in ducts were examined in a number of studies [20C,29C,30C]. The Graetz problem was considered for liquid metals [32C] and in rarified gas flows [2C]. Mixed forced and natural convection was examined by several authors. Unstable mixed convection was studied in bottom heated horizontal [17C] and inclined [18C] ducts; external boundary conditions were also addressed [13C]. Mixed convection in vertical tubes was studied [9C–12C]. Laminar heat transfer was investigated between parallel plates [26C] and in a vertical heated channel [21C]. Entrance effects were considered in He II flow [16C], in annular ducts under mixed convection [22C], in gas-cooled beam windows [28C], and for laminar forced convection [1C]. A finite volume method of lines was used to study turbulent forced convection in circular tubes [3C]; the numerical method SIMPLE-C was used to study mixed convection between parallel plates [4C]. Three-dimensional transient calculations were made for flow far downstream in a horizontal duct heated from below [5C]; entropy calculations were made for flow through a duct as a function of length [6C]. A numerical simulation of mixed convection was conducted [7C] as well as one in zero gravity for water near its critical point [14C,15C]. The upstream migration of heat was examined in a horizontal parallel plate duct [8C]. Heat

transfer analysis was undertaken using the axial moment method [31C] and through inverse analysis [19C,23C]. Flow and heat transfer in capillary tubes were studied for CFC-12 and HFC-134A [33C]; forced convection of FC-77 was also examined [25C]. Analytical velocity and temperature distributions were investigated for laminar flow for H2 boundary conditions [27C]. Combined buoyancy effects were addressed in horizontal rectangular ducts [34C] as well as low Mach number compressible flows [24C].

#### 4.2. Irregular geometries

Although the straight-walled duct is attractive as a testing ground for fundamental experimental work and computational methods, many practical situations fall into the category of irregular geometries. Heat transfer in a bayonet tube was studied for laminar flow [44C], during laminar-turbulent transition [43C], and for Prandtl number effects [42C]. Combined convection flow in a vertical eccentric annulus was studied over a range of parameters, including Grashof, Prandtl and Reynolds number [40C]. Flow diffusion and the accompanying heat transfer were investigated in an axisymmetric annular duct [48C] and in a pipe-expansion flow [39C]. Forced convection was also studied in microchannels; in one study water flow was examined [45C] and in another binary mixtures were considered [46C]. A numerical investigation of turbulent forced convection in rectangular and trapezoidal ducts was undertaken to assess the appropriateness of various turbulence models [47C]. A hexagonal lattice of circular tubes was examined using the manipulation system REDUCE [38C]. A finite element solution for forced convection heat transfer in plate-type monolith structures was done [37C]. Flow in a double-sine shaped duct for fully developed laminar flow was simulated using a Galerkin integral method [36C]; laminar mixed convection in a vertical elliptic duct was investigated using a control volume based numerical scheme [49C]. A simplified model for real gas expansion between two reservoirs was developed [35C] and the thermal development of radiatively active pipe flow was studied with nonaxisymmetric heat loss [41C].

#### 4.3. Finned and profiled ducts

Heat transfer augmentation is often achieved using protuberances of one type or another; the accompanying pressure drop penalty must also be addressed. Electronic packaging presents a practical environment where surface profiling is present and needs to be understood. Forced convective air cooling of electronic components was examined [58C]; the heat transfer and associated pressure drop was also addressed [63C]. A

comprehensive review of enhanced tubes was found in the literature [70C]. Thermally active and inactive perforated ribs were studied in a low-aspect ratio channel [62C] as well as in a 2D/3D rib-roughened annulus [75C]. The heat transfer and pressure drop in tubes with short turbulators was studied [64C]; an internally finned equilateral triangular duct was investigated experimentally [52C]. Analysis and performance comparisons of integrally enhanced tubes was conducted [71C] as was the laminar flow and heat transfer in internally finned tubes [73C]. The impact of artificial roughness on turbulent heat transfer coefficients was studied in the entrance region of a circular duct [66C]. Complementary experimental [74C] and numerical [56C] studies of heat transfer in corrugated passages were conducted. The disturbances and heat transfer effects caused by vortex generators were examined in a numerical and experimental study [51C]; a vortex generator placed above a rib was also studied [67C]. The role of multiple obstructions on conjugate forced heat transfer in tubes was addressed [72C]; general correlations for pressure drop and heat transfer in enhanced tubes with turbulent flow were found in the literature [69C]. Laminar flow in a circular duct with circumferential tubes was analyzed [68C] as well as one with inserted longitudinal strips [60C]. Local heat transfer coefficients were determined for flow over a ribbed surface [59C]; a converging passage with discrete ribs was also studied [61C]. The effect of size of a wire-screen matrix on a regenerator was examined in a cryocooler [53C]; the effect of tube-tape clearance in a horizontal isothermal tube was investigated experimentally [50C]. Single-phase heat transfer in microfin tubes was addressed [77C]. Numerical predictions of heat transfer augmentation in tubes with two-dimensional square ribs were presented [76C]. The impact of single roughness elements was investigated with a surface-mounted heated block [54C,55C]; the disturbing effect of fluid injection was also studied [57C]. The turbulent velocity and temperature characteristics in a heated rod bundle were documented [65C]. An experimental study was conducted to determine the heat transfer response to relative humidity in source arrays [78C].

#### 4.4. Duct flows with secondary motion

The most common flow studied in the literature during 1996 involving secondary motion was that in curved or helically coiled pipes. Effects of Dean vortex pairs on heat transfer were studied [86C] as well as the well-known relaminarization phenomenon [89C]. The secondary motion in helically coiled pipes was studied in air–water flows [90C], for finite pitch [79C] and for substantial pitch [91C]. Second moment closures were examined to handle the complicated three-dimensional

motion in a U-shaped tube [81C]. The analogies between turbulent flow in curved pipes and orthogonally rotating pipes were provided [82C]; the effect of Rossby number was investigated in rotating curved pipes [83C]. The secondary motion imposed by vortex flow was studied in a horizontal rectangular duct [87C]. Heat and mass transfer was examined in a serpentine channel with right-angle turns [80C] as well as in a curved pipe with a coaxial core [88C]. Streaming motion was studied in tube refrigerators [85C] and in transformer oil [84C].

#### 4.5. *Oscillatory and pulsatile flow*

A numerical study of turbulent forced convection in a periodically ribbed channel with oscillatory flow was achieved using a sinusoidally varying pressure gradient [93C]. The reciprocating flow and heat transfer in a circular pipe was studied in both instantaneous and cycle-averaged quantities [100C]. The oscillatory flow in baffled tubes was reviewed in the literature [97C]; flow mixing, heat transfer and mass transfer issues were considered. The forced turbulent convection between parallel plates experiencing sinusoidal inlet temperature variations was studied [92C], as well as the viscous dissipation and heat transfer in pulsatile flow of a yield-stress fluid [94C]; also see non-Newtonian fluids below. The effects of pulsation on internal heat transfer in a circular tube were addressed in an experimental study [95C]. A simplified analysis of the liquid oscillatory motion in circular pipes is provided based on experimental results [99C]. Discrepancies between mathematical and physical understanding of confined oscillatory flow was addressed using new parameters [96C]. The effect of small transverse accelerations on Bridgeman growth was also considered [98C].

#### 4.6. *Two-component duct flows*

Flows involving more than one phase or material are listed here and in a separate section in this review on two-phase flows; duct flows will be emphasized in this section. Air–water countercurrent flow was studied in a complementary theoretical and experimental study [105C]; air–water flow in a helically coiled pipe was investigated in terms of the Lockhart–Martinelli parameter [116C]. Heat transfer and friction data of R-22 and R-407C in a smooth tube for different evaporation pressures were presented [114C]. Phase distribution and heat transfer measurements were carried out in an n-heptane–water mixture flowing upward in a vertical tube [110C]; condensation heat transfer in a smooth horizontal tube with R-32 and R32/125 mixtures was studied experimentally [104C]. Fluid-to-particle heat transfer coefficients were evaluated in an aseptic pro-

cessing holding tube simulator [102C]; dimensionless correlations in the tube simulator were also explored [101C]. A wave front perturbation method was employed to examine two-phase flow in a horizontal channel [115C], and water–felspar flow through a vertical annuli was studied experimentally [113C]. The heat transfer and pressure drop for air–water mixtures was investigated experimentally in an isoflux vertical annulus [108C]. Gas–particle thermal interactions were examined in the presence of a surface [111C] and in the Tokamak type reactor [107C]. Modeling of volcanic eruptions was done in a finite rigid channel, using pressure driven flow [112C]. Heat transfer during gas hydrate formation in gas–liquid slug flow was modeled [106C]; the thermal performance of a phase-change material during cooling was mathematically modeled [109C]. A remote temperature sensor was used to evaluate the convective heat transfer between a fluid and particle in a continuous tube flow [103C].

#### 4.7. *NonNewtonian duct flow*

The heat and mass transfer occurring during solidification of waxy crude oils was studied [126C]. Shear-rate dependent thermal conductive of certain nonNewtonian fluids leads to heat transfer enhancement; analytical results were presented [125C]. The viscoelastic behavior of a fluid represented by the Criminale–Ericksen–Filbey constitutive equations was studied under laminar conditions in a rectangular duct [122C]. A finite element method was used to investigate a highly viscous nonNewtonian power-law fluid in a vertical tube [124C]. The thermal convection for Herschel–Bulkley fluids was studied numerically and experimentally in an annular duct [123C]. The viscoelasticity of a surfactant and its ability to affect drag and heat transfer were examined [121C]. Aqueous carboxymethylcellulose solutions were studied under laminar flow conditions in a square duct [120C]. The fluid mechanics and heat transfer of rheologically complex fluids were investigated during a chaotic mixing process [119C]. Power-law fluids inside ducts with catalytic reactions were studied; Sherwood number results are presented [118C]. It was shown that the Nusselt number distribution along the wall of an equilateral triangular duct depended appreciably on the power law index [117C]; the fully developed flow of a power-law fluid was modeled using finite element analysis in a rectangular duct [127C].

#### 4.8. *Miscellaneous duct flow*

A variety of studies could be characterized by their unique geometry, fluid type or application; this diverse group of papers will be summarized here. Turbulent

scalar transport was modeled using second-moment closure; various Prandtl numbers were investigated [141C]. An experimental heat transfer study, done in a metal hydride thermal energy conversion system, examined the interactions between two coupled reactors [134C]. The challenges posed during the disposal of heat-emitting waste was studied; argillaceous rocks were used as a test medium [132C]. The annular gas flow in a gas-lift well was presented through a mechanistic model [131C]. The cooling of aircraft skin made necessary by high-powered electronics was investigated; the analysis showed that skin cooling was a viable solution for heat dissipation from aircraft [129C]. An analytical model was presented to capture the dynamics of circulating fluid temperatures in drilling operations [133C]. Transient experiments were conducted to study the coupled natural convection in circulation loops [130C]. The governing equations describing the axial temperature variations in three-channel split-flow heat exchangers were presented and analyzed [135C]. The cool-down process of a demountable liquid nitrogen transfer line was studied experimentally; multilayer-insulated lines were addressed [136C]. The transient behavior of He II heated along the center of a pipe is treated numerically [138C]. Three turbulent models were compared for the application to tilting-pad journal bearings [128C]. The delay hot/cold water problem in fluid-pipe systems was examined [140C]. Generalized rib-tube correlations are used to optimize the roughness used for large evaporators and condensers [139C]. Heat transfer enhancement in an air compressor aftercooler was studied experimentally; the mechanism of heat transfer augmentation of a transversely corrugated tube was discussed [137C].

## 5. Flow with separated regions

Heat transfer in velocity fields dominated by flow separation are discussed in this section of the review. The most common configuration examined includes the broad class of flows past single cylinders or bluff obstructions. The extension of a cylinder from a plane wall was studied numerically; Nusselt number and drag results were presented [24D]. The heat transfer rates at the base of five basic geometries (cylinder, cube, diamond, pyramid and hemisphere) were compared; the effect of a single roughness element was also considered [6D]. The nonequilibrium airflow over a hemisphere was computed to examine hypersonic flow conditions [12D]. The impact of a splitter plane on a circular cylinder was studied under laminar flow conditions [18D]; heat transfer augmentation and Strouhal number were investigated. Tandem arrangements of

bluff bodies were treated for prisms [7D] and rectangular cylinders [22D]. The optimal spacing between cylinders in cross flow was studied using complementary analytical, numerical and experimental techniques [21D]. A numerical investigation considered the mixed convection past in-line cylinder bundles [13D]; results compared well with existing literature. Flow past a slender body at incidence and the associated heat transfer were examined analytically [25D]. The incipient separation of a turbulent hypersonic boundary layer was also studied at Mach 5 [3D]; nose-tip surface heat transfer mechanisms were studied under hypersonic flow conditions [11D]. An improved  $k-\epsilon$  model for low-Reynolds number flows was presented [20D] and compared to existing experimental and DNS data. The corner recirculating zone in a backward facing step was studied numerically [14D]; the effect of transverse curvature in a axisymmetric backward facing step was also considered [16D]. Forward facing steps were investigated under laminar natural convection flow [1D] and buoyancy opposed flow [2D]. Analytical expressions for the laminar flow in a circular step bearing and the associated temperature distribution under adiabatic conditions were presented [4D]. The unique flow in a double-circuit vortex tube was studied experimentally; applications of the work were also presented [19D]. One paper dealt with the laminar heat and fluid flow in a array of subchannels placed in a uniform stream [5D]. A modeling study was found which examined the characteristics of heat and mass transfer experienced in a deep-frying slab, cylindrical and spherical food products [8D]; a complementary study considered the drying of solid objects [9D]. A fast false implicit transient scheme was developed to predict the two-dimensional steady-state solutions of buoyancy-assisted laminar internal flows [10D]; a backward facing step was considered as a test geometry. Convective heat transfer from a cylinder experiencing surface reactions was examined [17D]. The time-dependent electromagnetic heat transfer equations were solved to study hyperthermic treatment [15D]. Step-wise pulse current/heat through horizontally immersed thin wires in helium II was also studied [23D].

## 6. Heat transfer in porous media

### 6.1. Property determinations

Several studies have reported attempts to better characterize a porous medium undergoing heat and mass transfer. The possibility of describing the structural characteristics of porous media via an information entropy parameter has been developed [15DP]. The accurate description of the flow field in a porous

medium was investigated via the use of a generalized velocity to which all other transport velocities are referenced [5DP] and via a domain decomposition method [10DP]. A theory for flow and heat transport in deformable porous materials has been developed by [7DP,8DP].

The influence of the initial concentration of solute and super-cooling on permeability of a porous medium saturated with a partially solidified aqueous solution was determined via transient methods [12DP]. The relative permeability of relations for vapor and liquids for capillary porous media were deduced from a combination of numerical and experimental studies and found to be based on the capillary pressure which can be measured. [2DP]. The permeability and dispersivities of solute and heat for a porous medium were determined computationally using a theoretical construct that accounts for the mobility ratio of gas and liquid in unsaturated systems [1DP].

Thermal conductivity at high temperatures in porous Ni/yttrium-stabilized zirconia cermets was determined via flash laser heating and application of the effective medium theory [6DP]. The laser flash method was also used to verify predictions of effective conductivity based on a simulation of the microstructure [11DP]. Some very fundamental experiments on transient heat transfer indicated that neither a wave or pure diffusion model can adequately explain the observed temperature and thermal penetration depths as a function of time [14DP]. The dependency of thermal conductivity on gas pressure and temperature was investigated in materials with porosity greater than 30% [9DP]. A procedure for determining the moisture diffusivity using moisture concentration profiles was developed and quantified [13DP]. A primary source of uncertainty in reported values was inhomogeneity of the matrix.

Modeling based on Luikov's heat, mass and pressure transfer system in a capillary porous body was used to estimate thermal and moisture conductivity [4DP]. The effects of surface segregation kinetics and pore size on effective thermal conductivity of porous ceramics was modeled to predict the dependence of the thermal conductivity on the material thermal history [3DP].

## 6.2. Fluidized beds

Basic and applied studies of fluidized beds, as a special category of porous medium, continue at a goodly rate. Applied studies this past year tend to emphasize the performance and the of the bed within a given range of operating parameters. More fundamental studies have investigated better characterization of heat /mass transfer and hydrodynamics within the bed, and scale up from laboratory experiments.

A two-fluid model of bed hydrodynamics was developed for the dense phase system [23DP]. The hydrodynamics of fast fluidization has been extensively reviewed, and a scaleable mechanistic model of heat transfer for which the primary parameter is the bed suspension density is found useful [18DP]. Conductivity and salt tracer measurements have been used to provide local holdup and circulation patterns of the liquid and solid phases [26DP], and gamma-ray transmission measurements were used to map the maximum void fraction in a heat-generating system [33DP]. Experiments have been run and compared with models of pulsed beds used in drying and for heat transfer [24DP], and a model for unsteady heat transfer in an air cooled bed was developed [20DP]. The influence of wall roughness on bed hydrodynamics was studied experimentally [42DP]. An analytical model to determine particle-to-surface temperature distributions using available point wise average heat transfer measurements was developed and validated [22DP]. The Zadbodsky correlation for heat transfer in a bubbling bed has been modified for a recirculating bed [39DP,40DP]. Flow visualization of flowing particles around imbedded tubes was conducted via X-ray video films to determine the relation between particle behavior and local heat-transfer coefficients [37DP], and measurements were presented for a heated probe in a magnetofluidized bed [35DP].

A simple model has been developed for bed heat transfer dependent on input parameters, including mass flow of particles and flue gases [25DP]. A modified cluster renewal model has been developed for heat transfer in pressurized beds [17DP]. Heat transfer to several types of immersed surfaces was investigated experimentally [27DP–30DP,36DP]. Coupled heat and mass transfer were experimentally investigated to determine effects of bed height, gas velocity, initial moisture content, and air temperature [21DP].

In several special studies, a hybrid neural model of the dewatering process has been developed [41DP], temperature and composition was predicted in a jetting fluid bed gassifier [19DP], and a mechanical fluidized vacuum furnace was developed [16DP]. Thermal entrance effects for heat transfer in up-flowing gas-particle suspension was studied experimentally [38DP].

Fluid bed combustors were investigated to determine the sintering tendency of ash produced [32DP] and factors affecting the devolatilization of coal [34DP]. A systems model of the use of a fluid bed combustor in concert with a gas turbine for repowering a steam plant was studied to determine an optimal system configuration [31DP].

### 6.3. Free convection

The stability of conduction regime in saturated porous layers was investigated for the case of a porous layer lying under a fluid layers [56DP,54DP]. Stability criteria have been developed for the translucent layer with radiative heat transfer [62DP] and for layers in which the body force alternates in direction [65DP]. All of these studies are variations of the more familiar Rayleigh–Benard problem extended to porous layers.

Research on free convection in a fully saturated porous media continues to be of interest from the fundamental perspective. A number of new problem types have begun to appear in the literature, and most of the them are driven by specific technological applications. The general enclosure problem, including rectangular cavities, annuli, and slots has been investigated for steady state heat transfer under either the traditional Darcy–Boussinesq approximations or formulations that take into account nonlinear viscous effects [47DP–51DP,60DP]. Enclosures of complex geometry have also been considered in this context [59DP]. The special case of an enclosure partly filled with a porous medium and single phase fluid was investigated [61DP, 58DP]. Double diffusive convection in an enclosure has been addressed, also numerically, via an extended Darcy formulation. Transient convection in enclosures driven by either time-dependent thermal boundary conditions or vibrational excitation have also been reported [43DP,55DP,57DP].

Heat transfer from surfaces and bodies imbedded in a saturated porous medium has been studied for uniform and nonuniform thermal boundary conditions. The flat plate problem has been addressed for steady [63DP,64DP] and transient [45DP,46DP,52DP] thermal boundary conditions. Special cases as variations of the standard Darcy formulation included convection in nonNewton fluids [67DP], on a slowly rotating imbedded cylinder [68DP], and in a viscous, electrically conducting and heat generating fluid [66DP]. An interesting model for the enhancement of heat transfer rates from an array of discrete heat sources was presented [53DP], and the effect of porous coating materials on heat transfer from a surface was investigated experimentally [44DP].

### 6.4. Coupled heat and mass transfer

Fundamental studies of coupled heat and mass transfer in porous media has occupied a significant fraction of the literature during the past year. For many of the articles selected for this review, categorization is not easy given the similarities that exist in the formulation of the governing equations for a wide range of applications. Further, modern computational

techniques and the power of modern computers have helped blur the distinctions that have are usually made among research activities in this field. For example, fundamental studies of drying processes and three-phase transport in packed beds are beginning to take on a commonality that hitherto has not been seen. In addition to the traditional motivations to better understand rate processes at a basic level in packed beds and drying, transport in soil related to sub-surface remediation, and the prediction of pollutant movement have received attention.

The use of the concept of “matrix replenishment” in relation to matrix diffusion has been introduced for the complex problem of contaminant transport in non-isothermal fractured porous media [70DP]. A special apparatus has been developed to study time-dependent heat and moisture transfer in fibrous insulation under heat conduction with water vapor adsorption/desorption, condensation and frosting [79DP]. Time-dependent transport has been analyzed with porosity changes due to dissolution of the solid matrix. [72DP]. Coupled heat and mass transfer has been studied with an emphasis on the effect of matrix structure [81DP]. Convective burning as a precursor to detonation of granular beds was studied experimentally for the special case of low porosity beds; a primary finding was that low velocity convection and compaction are major factors for low porosity beds [69DP].

The effects of initial moisture distribution on transient heat flow through wet porous material was with variable thermophysical properties was studied experimentally and numerically [86DP,87DP]. A boundary layer analysis of combined heat and mass transfer by natural convection from a concentrated source in a saturated medium for both line and point sources was reported [76DP]. An approximate solution for oscillatory flow past a porous plate was presented for variable suction and species transport [80DP].

An advanced formulation of multi-component, multi-phase transport in capillary porous media has been developed and applied to the simulation of the transport of organic compounds in a subsurface environment [83DP,71DP]. This work has produced a mathematical model of multi-component, multi-phase transport that is economical in terms of computational time. A mathematically interesting analysis of liquid, vapor and gas flow has been developed which allows three values of saturation for a given flux of mass, energy and gas [85DP]. An exact solution of coupled heat and mass transfer with moisture desorption under temperature gradients in a vacuum environment was also obtained [78DP].

For the problem of thermo-hydro-mechanical analysis of coupled heat, water and gas flow in a deformable porous medium, a parallel Newton–Raphson algorithm has been developed that is solved using net-

worked workstation-level computers [84DP], and a hybrid finite difference and finite element solution has been tested against experiments on partially saturated soil and clays [75DP]. A two-dimensional finite element solution was developed for heat and mass transfer in irrigated soils and validated against field measurements [77DP]. The special case of cylindrical heat sources in a saturated elastic saturated medium has been presented [82DP]. A microbial landfill ecosystem has been modeled as a porous medium to determine the transport of heat and mass [73DP,74DP].

### 6.5. Drying processes

Studies of drying processes have expanded somewhat to include both high and low heat flux applications. A comprehensive review of steam drying has been presented by [98DP].

One study focuses on modeling the drying and eventual spalling of a concrete wall exposed to fire [88DP], and others presented a model for combined drying and pyrolysis of hygroscopic material, such as wood [93DP,91DP]. For the early stages of drying in initially saturated concrete, it was found experimentally that diffusion control sets in when the moisture content decreased below 80% of initial saturation [95DP].

Convective drying has been studied via modeling and experimentation. An empirical relation between Nusselt and Sherwood numbers and the Reynolds and Gukmann numbers developed for single, short porous cylinders [96DP]. A one-dimensional analysis for temperature and moisture variations was developed and verified for brick and mortar [94DP]. Convective drying in the presence of solar thermal radiation was modeled and studied experimentally [92DP]. Two-dimensional effects on the drying of plates in forced convection were determined experimentally [90DP].

The drying of food materials has been approached by a combination of experimental and theoretical studies. An experimentally validated model uses Luikov's equations for capillary porous media and applies it to constant pressure in during of hydrated composite starch [99DP]. An experimental study of drying of dense pasta suggests that diffusion dominates mass transfer during the entire process [97DP]. A model of drying due to micro-wave heating of granular hygroscopic solid was found to be sensitive to initial moisture content, size and heat transfer coefficient [89DP].

### 6.6. Multiphase flow and heat transfer

An experimental study was reported for transient regime heat transfer with liquid-vapor phase change in forced flow and compared to a model that predicts the boundaries the two phase and vapor zones [107DP].

The influence of sorption isotherms on the transport of liquid and vapor was studied using a mass transfer coefficient and a specific evaporating surface [109DP]. Laboratory experiments were conducted on constant pressure steam injection and transient condensing flow in an air-saturated medium; the propagation of the steam front appears to be proportional to the square root of time [100DP].

Liquid film evaporation in heated gas flow in a contact apparatus was investigated experimentally, and flooding criteria were reported [101DP]. Condensation processes under random fluctuation of ambient temperatures as conducted to develop a probability density of the moisture content [103DP]. The dryout of a bed of volumetrically heated particles cooled by a two-phase flow with evaporation was investigated to predict dryout limits for shallow and deep beds [104DP,105DP].

Three-phase flow in a catalytic reactor was modeled for co-current flow of liquid and gas to determine liquid–solid and gas–liquid mass transfer coefficients [108DP]. Two major hydrodynamic regimes were identified for heat transfer in co-current gas–liquid flow in a packed bed reactor [106DP,102DP].

### 6.7. Forced/mixed convection in stationary beds

Forced convection — Most of the literature on forced and mixed convection in stationary (packed) beds has dealt with experimental and theoretical studies that have broadened the knowledge base by either extending or sharpening correlations for transport transfer coefficients. Several studies have also been aimed at refining fully analytical and semi-empirical transport models. A comprehensive review of the subject has been published [126DP]. A few studies have focused on developing flow, heat transfer and flow stability [128DP,148DP,129DP], and flow past an imbedded object [143DP]. The analysis of the flow of a free surface and of two fluids in a porous channel was also presented [118DP]. The special case of forced convection from a porous block mounted from a heated wall in laminar flow was computed using a one-equation model for energy and Van Driest's wall function [123DP].

The fundamental problem of predicting heat transfer from a single phase fluid to a stationary packed bed has been formulated as a system of equations that pertain to the fluid and solid phases [113DP, 121DP,134DP,136DP,122DP]. Solution methods vary but all of them bear a close relation to the problem of predicting effective values of the transport coefficients. Other very fundamental studies include solutions for heat transfer in a saturated porous channel, or slot, with isothermal or isoflux boundaries [140DP,111DP,

131DP,130DP] and characterization of heat transfer and pressure loss [119DP]. Wall heat transfer coefficients for a packed bed with tube-to-particle diameter ratio of approximately two were computed for low Reynolds number flow and found to be in good agreement with measurements [120DP]. An empirical correlation for average Nusselt number in a pipe packed with rigid spheres has been developed for the Darcy, Forcheimer, and turbulent regimes of flow [147DP]. The reduction of the wall effect on heat transfer in a packed was demonstrated using a liner sheet comprising convex hemispheres [141DP].

The effect of a variation of the structure of the porous matrix on forced convection received special attention through both experimental and analytical/numerical investigations [142DP,126DP,145DP,127DP,137DP]. Nonsaturated media has also been treated numerically [144DP]. A turbulence model for flow through porous media using a volume averaging technique, effective eddy diffusivity, and the 0-equation model was developed [138DP].

The control and time-dependent behavior of packed beds under periodic and pulsed flow conditions were also modeled [139DP,112DP]. The response of a packed bed for a step input was determined via a three-dimensional perturbation method [135DP]. The high Peclet number limit for heat and mass transfer in a packed bed was also investigated [132DP]. Stagnation point flow of a chemically reactive fluid in a catalytic bed was analyzed for both transient and steady flows [115DP]. The dilution of a catalyst bead was studied via small-scale and scaled-up laboratory units to improve heat transfer and improve the overall effectiveness of the bed [146DP].

Mixed convection — Studies of mixed convection on stationary porous beds have begun to appear as applications for high porosity materials have developed. Heat transfer from horizontal and vertical walls is being investigated to determine the effects of nonDarcian phenomena on heat transfer coefficients [133DP,124DP,116DP,117DP]. Heat transfer for non-Newtonian fluids is also of interest [125DP]. Developing flow and heat transfer in channels partially filled with porous media has been solved using a hybrid scheme for convection and diffusion [114DP]. Mixed convection heat transfer coefficients on an imbedded cylinder were computed for nonDarcy flow [110DP].

## 7. Experimental techniques and instrumentation

Many experimental results are cited in other categories of this review. The purpose of this section is to

identify papers that focus on new or improved experimental measurement techniques or devices that are useful in experimental studies of heat transfer. The publications referenced here deal explicitly with some aspect of heat transfer measurement or include a general review of techniques that are applicable to heat transfer measurements.

### 7.1. Heat flux measurements

A review of methods applied to combustion was presented [1E]. The directional sensitivity of a wall-mounted hot film gauge with respect to yaw angle was determined [3E]. A new type of thin foil radiometer was described [4E] that measures the net radiative flux on a surface. The application of a water-cooled calorimeter to the measurements taken in a pool fire were described [6E]. Methods to measure heat transfer coefficients were also presented [2E,5E].

### 7.2. Temperature measurements

Thin film thermocouples developed for warm turbine testing were discussed [14E]. Transient temperature measurement sensors were described [16E,19E]. Liquid crystals have been applied to transient temperature measurements in hypersonic flows [7E] and near cavities on a flat plate [10E]. Accelerations up to 16,000 *g* were found to have a negligible effect on liquid crystal performance [20E]. Noncontact temperature techniques and sensors include holographic interferometry [17E], infrared radiometers [12E,13E], a scanning thermal microscope [15E], and others [8E,9E]. Temperature measurements have been made on various tissues [11E,21E]. The temperature of fiber tips used in scanning microscopy were measured to understand the process of tip heating [18E].

### 7.3. Velocity measurements

Studies of hot wire anemometers include a discussion of the different metrological problems encountered in turbulent flows [22E], the development of a pulse heated anemometer [24E], the use of four-wire probes in vorticity measurements [25E] and the angular response of an x-wire probe at low velocities less than 1.4 m/s [26E]. Zhang et al. [27E] discuss three intermittency measurement methods applied to transitional boundary layer flows. An impervious heated cylinder has been used as a ground water velocimeter [23E].

### 7.4. Thermophysical property measurements

Various methods were developed to measure properties in solids including thermal conductivity [31E], ther-



mal conductivity and heat capacity [28E], and thermal diffusivity [29E]. A transient hot-wire method was described that can determine thermal conductivity and thermal diffusivity of liquid simultaneously [30E].

### 7.5. Miscellaneous methods

The use of two-point laser Rayleigh spectroscopy to determine space and time-resolved structures of turbulent diffusion flames was discussed [33E]. Reviews of low cost sensors [34E] and magnetic resonance imaging applications [32E] were presented.

## 8. Natural convection — internal flows

Natural, or free convection, continues to evolve as a subject for both basic and applied research. The fundamental literature this year has shown growth in the direction of systems in which buoyancy exists in concert with external forcing conditions and/or nonuniform thermal boundary conditions. However, very fundamental studies of heat transfer in layers, cavities, and channels yet dominate published research. There is a growing interest in describing buoyancy dominated flows in systems with forcing conditions applied either at the boundary or volumetrically. The development of new industrial processes, such as in materials manufacture, and in space processing motivate this research.

The literature on heat transfer phenomena associated with fires also continues to grow. Increasingly, studies of fire and its related transport phenomena are aimed at quantifying mechanisms of initiation and spread in both pools and enclosed spaces. The general directions of the research on fires and related natural convective phenomena has produced a literature that can be conveniently categorized. Major areas of research focus are: (1) Modeling and experimentation to determine and describe transport phenomena; (2) experimentation and large-scale testing to support model development; (3) validation of production codes and their internal transport models; and (4) verification of production codes.

### 8.1. Plane layers

Rayleigh–Benard convection was investigated numerically and experimentally for a system comprising two immiscible liquids for a range of buoyancy ratios and thermal boundary conditions [6F,4F,2F]. Fundamental aspects of environmental flows were also investigated for high Prandtl number fluids, including the dynamics of thermal release and the effects of temperature-dependent viscosity [5F,7F]. An interesting experimental study of steady state heat transfer in air layers

heated from above reports heat transfer relations and flow field information for two aspect ratios and inclinations [1F]. A fundamental experimental study of penetrative flow due in a stable double layer system due to an immersed isothermal wall shows that penetrative flows result from the interaction of oppositely directed flows that meet and mix at the interface [3F].

### 8.2. Cavities

While most studies reported for cavities of moderate aspect ratios were numerical in nature, some important experiments were published. Nusselt numbers at very high Rayleigh number were measured by Chavanne et al. [12F], with the  $Nu$ -vs.- $Ra$  relation showing a departure from the  $2/7$ -ths power law above  $Ra \sim 1E+10$ . Two detailed studies of the structure and evolution of transient convection via flow visualization in square and rectangular cavities with heating from the side walls were reported [14F,19F]. The structure of the two-dimensional flow fields for various aspect ratios and heating from either the side walls or the bottom yet draws attention, with computational schemes and details of the flow being simultaneous foci of reported studies [26F,16F,25F,8F]. The three-dimensional flow in a cubical cavity heated from below was computed [19F] to reveal the existence of four stable structures for  $Ra < 1E+04$ , and flow transitions for two- and three-dimensional perturbations were also determined numerically [13F,15F]. For a cylindrical cavity [17F], a series of roll and open roll flows dominate for Rayleigh numbers moderately elevated above the critical value for the onset of motion.

Cavities with complex thermal boundary conditions are also receiving systematic treatment. Convection driven by partially heated boundaries reveals flow and temperature fields with oscillatory and periodic behavior [20F,21F,27F]. Experimental data for temperature and flow fields in a long box driven by nonuniform heating and cooling on the horizontal boundaries were reported [24F]. Some interesting results for inclined cavities were also reported for both application to solar energy engineering and end-driven flows [18F,23F].

Some interest has also been shown in the special case where buoyancy forces are produced via volumetric heat release within the convecting fluid. Two experimental studies of convection with nuclear reactor technology and post-accident heat removal have been reported for a volumetrically heated segment of a sphere that is cooled externally from the curved surface [9F,10F]. On a more fundamental level, the effects of a sinusoidally varying heat source in a square cavity were investigated numerically [11F]. The stability of a uniformly heated fluid layer continued to receive some

attention but added complexity due to convective and other types of boundary conditions [22F].

### 8.3. Conjugate problems

Natural convection in which the system boundaries couple thermally to the fluid continue to receive attention, though not the extent that one would expect. Conjugate convection between two fluids separated by a horizontal wall was investigated both numerically and analytically [31F]; the related problem for channel flows with discrete heating was reported by [28F]. Buoyant conjugate heat transfer in horizontal planar thermosyphons was thoroughly analyzed by [29F,30F].

### 8.4. Vertical channels and slots

Fundamental work on vertical channels and slots this past included several studies that provide measurements of velocity and temperature fields for important engineering applications and for validation benchmarks for theoretical studies. Such experiments have been reported for a tall cavity with air as the working fluid [32F]. A mass transfer analog has also been investigated [39F].

For very high Prandtl number fluids in a differentially heated slot with aspect ratio 15, [35F,36F] report temperature and velocity fields in good agreement with recent experimental results. With air as the working fluid in either a slot or channel, several finite difference studies report velocity and temperature fields [33F,37F,38F]. For a slot with discrete heating, a fully analytical solution for the velocity and temperature fields is able to reveal the energy content of the dominant modes of flow [34F].

### 8.5. Annular flows

Vertical and horizontal annuli were the objects of several studies. Numerical work was reported for constant flux heating on the inner wall for a tall but finite annulus [46F] and for the horizontal annulus with water at the working fluid [45F]. Systems with eccentric cylinders and a noncircular outer wall were also considered via numerical analysis [44F,41F]. Experimental and numerical results for heat transfer were presented for a vertical annulus with an adiabatic upper boundary [43F]. An interesting analytical study of flow stability in a tall vertical annulus was reported for a range of Prandtl numbers and disturbance modes [40F]. A numerical investigation of convection between concentric and vertically eccentric spheres with mixed boundary conditions showed that heat transfer coefficients and flow fields mainly depend on the Raleigh number and the eccentricity [42F].

### 8.6. Complex geometries

A variety of applications has motivated experimental and numerical work on buoyancy driven flow in complex enclosures. A combined numerical and experimental modeling technique has been suggested for imperfectly mixed fluids in a ventilated space [49F]. Flow patterns and temperature fields in partitioned enclosures were investigated for very large Rayleigh numbers using three- and four-equation models for turbulent transport [51F]. Cavity flows driven by heated parallel plates within the enclosures were numerically determined [52F]. Experiments and analysis for a horizontal open annulus were reported [50F], and experiments were conducted on horizontal enclosed rod bundle [47F]. A parametric study for flow and heat transfer in L-shaped corners with asymmetric heating was reported [48F]. The enclosure with conducting multiple partitions received attention, and some progress was made toward a generalized representation of the problem [54F]. Buoyancy driven flow and heat transfer from helicoidal pipes was investigated experimentally, with the key finding being that local and average Nusselt numbers for the horizontal coil being larger than those for the vertical coil [55F]. An experimental and numerical investigation of coupled convection and diffusion in a U-tube reactor was able to accurately predict the mixing of reactants prior to the onset of global convection [53F].

### 8.7. Transient systems

An interesting feature of this year's literature has been the appearance of a variety of studies on buoyancy affected flows wherein buoyant forces are coupled to external forcing conditions. Such forcing conditions may be transients imposed at the boundaries of the system, vibrational effects, or oscillatory bulk flows. A primary category of research in this broad category includes experimental and numerical studies for cavities with time-varying thermal boundary conditions [57F,61F]. Instability in a differentially heated flat, inclined layer subject to high frequency vibration was studied analytical and numerically for small amplitude, two-dimensional disturbances for all combinations of temperature gradient and axis of vibration [58F]. Resonance in thermo-vibrational convection was observed via numerical studies [59F]. Convection with physically moving boundaries, so called lid-driven flows, was studied both experimentally and numerically [56F,62F]. As flow in this category leads easily to mixed convective situations, a related study is that in which oscillatory pressure gradients exist in a channel with bottom wall heating [60F].

### 8.8. Plumes and thermal discharges

Research on buoyant plumes of several types has been motivated both by technological and environmental problems. An experimental and theoretical study of a wall plume arising from a thermal source on an inclined surface has been reported along with a correlation for Nusselt number over a wide range of Prandtl numbers and angles of incline [64F]. On a larger scale, studies of simple heat islands, which are a special class of the urban heat island, were performed using small scale laboratory models [65F]. Some new data on self-preserving plumes were also reported [63F]. A verification of dilution in environmental thermal discharges using the US EPA's CORMIX2 and UM production codes was also reported [66F]. The two codes demonstrated some difference in overall predictions for selected case studies.

### 8.9. Double diffusive and thermocapillary convection

Double diffusive convection in enclosures continues to be investigated numerically and analytically. Various studies were reported that continue to describe heat transfer and flow structure [72F,70F]. General mass transfer relations are also proposed, and the influence of the interactions between density differences and thermal gradients are elucidated [67F,69F].

Thermocapillary effects on natural convection had drawn attention via both experimental and numerical studies. Oscillatory flows in cylindrical systems [71F] were investigated experimentally for both heat transfer and flow field. Transient flows in multi-fluid layers [74F] were investigated numerically, and oscillatory flows were found for large Rayleigh and Marangoni numbers. A numerical study of an evaporating axisymmetric droplet predicts that surface tension strengthens internal circulation and thereby shortens overall evaporation time [73F]. For a system comprising two superposed fluid layers under reduced gravity, thermocapillary forces are seen to play a role in the heat transport process under micro-gravity conditions [68F].

### 8.10. Fires

The validation and use of fluid dynamics and specialized heat transfer (CFD/CHT) codes have been the focus of several papers on tunnel and room fires [98F,99F,84F,82F,76F]. Separate heat transfer effects, e.g., radiative heat transfer, convective heat transfer, etc., and the propagation of the fire were of greatest concern. Zonal models of fires in rooms and buildings continue to occupy a goodly fraction of the work underway to accurately exercise production codes.

CFD/CHT commercial codes were also used to assess the effectiveness of extinguishment of enclosed gas fires by a water spray [88F]. Fundamental model development has been directed at dehydration and stress analysis [77F], coupled heat and mass transfer in woodland fires [86F], wood combustion [87F], and heat transfer in composite wall structures [97F]. All of this work involves a goodly number of approximations and generally the solution of the coupled equations for heat and mass transfer.

More fundamental model development work has also been done this past year. Typical studies are those involved in the design of steel-framed walls [85F], developing constitutive relations for steel at high temperature [93F], and overall thermo-structural analysis [78F].

Work on fire dynamics involved both numerical and experimental work. Poreh and Morgan [90F] have developed a homogeneous power law to describe the vertical variation of mass flux in the near field of turbulent flames and plumes. The ignition of a flammable pool was idealized as liquid layer with a focused heat flux on the upper surface; the problem is mathematically modeled as a nonlinear conduction problem [81F]. Buoyant flows related to fires in enclosed and partially enclosed spaces were investigated numerically for both laminar and turbulent flows [75F,91F,100F].

Large scale fires and their assessment were carried out on ignition, spread, and interactions with structures. Flame spread in composite materials were reported [89F,83F,95F], and the effects of ignition sources on heat release from upholstered furniture were measured [94F]. Assessment of large scale tests addressed stratification in fuel tanks [79F], fire resistance and endurance parameters [96F,80F]. A critical assessment was presented by [92F] on the use of the cone calorimeter in the analysis of fires.

## 9. Natural convection — external flows

### 9.1. Vertical plate

Studies on buoyancy driven convection heat transfer from a vertical plate include the influence of a transverse magnetic field under microgravity conditions [9FF], transient mass transfer in a steady laminar flow [10FF] and unsteady heat transfer over a continuous moving vertical sheet at constant surface temperature and constant surface heat flux boundary conditions [7FF]. Studies of convection of a nonNewtonian fluid on a wavy vertical plate has been analyzed including the influence of a magnetic field [1FF,16FF]. Conjugate natural convection from a vertical plate has been analyzed using a finite-difference scheme [11FF] and

using numerical and asymptotic solutions [15FF]. Other studies of natural convection on a vertical plate include the use of an algebraic flux model to study turbulent heat transport [2FF] and a numerical model for studying heat transport with a phase change material [3FF]. Combined mass and heat transfer with multi component electrochemical systems [5FF] and with double diffusive convection [12FF] have been analyzed. A special case concerns convection from a draining film with thermocapillary instabilities [6FF]. Laser holographic interferometry was used to study convection from vertical rectangular fins [8FF] while a numerical solution established optimum fin spacing for heat sinks [13FF]. Protruding blocks on vertical surfaces have been studied experimentally [14FF] and numerically [4FF] to simulate heat flow from computer chips.

### 9.2. Inclined and horizontal surfaces

A boundary layer analysis provides heat transfer results for convection of a micropolar fluid on a horizontal plate [18FF]. Boundary layer flow with a variable viscosity fluid and free surfaces has been described [17FF]. An asymptotic analysis predicts thermal ignition of combustion gases [19FF] flowing along an inclined surface.

### 9.3. Spheres and cylinders

Several studies examine convection from spherical systems. Steady [23FF] and transient [24FF] laminar convection from spheres has been studied over a large range of Rayleigh and Prandtl numbers; potential flow, separation and a recirculation vortex are discussed. Cooling of spherically shaped melons was studied experimentally under time varying conditions [21FF]. A horizontal surface near a horizontal cylinder can change the convection flow pattern [25FF]. Experiments and analysis provide the effect of shape of horizontal elliptical cylinders on the mean heat transfer [20FF]. Numerical studies show the increase in heat transfer from a cylinder due to the presence of multiple low conductivity longitudinal baffles [22FF].

### 9.4. Mixed convection

A number of studies consider heat transfer with both buoyancy-driven and forced flows. A model provides good agreement with the experimental data for a vertical plate in which the forced and natural convection flows are either in the same or opposing directions [28FF] while a related study [32FF] converts the model to similar flows on circular discs. Experiments on the face of an eight storey building provide data for mixed

convection heat transfer to apply in the design of multi-storey building structures [29FF]. Similarity solutions are provided for mixed convection on a continuous flat plate with a fluid whose viscosity is dependent on temperature [27FF]. Other mixed convection studies include analyses for flow of a micropolar fluid in the axisymmetric stagnation region of a vertical cylinder [26FF,30FF] and for flow around a heated cylinder mounted between parallel plates [31FF].

### 9.5. Miscellaneous

Use of triangular elements in a finite element analysis provides rapid convergence of the numerical solution for several different geometries over a range of laminar flow Rayleigh numbers [38FF]. A boundary element method provides two-dimensional time-varying heat transfer data for oscillatory natural convection [39FF]. A model [33FF] predicts the influence of natural convection on measurement of the diffusion coefficient in concentrated liquid alloys. Convection studies include simulation models for the growth of single crystals of cadmium telluride [40FF]. Under microgravity conditions the influence of thermo-acoustic convection [41FF] and a model for dendritic growth [37FF] have been discussed. Natural convection effects on the temperature distribution in gravel embankments over summer and winter seasons [35FF], the heat transfer and flow in models for storage of reactor fuel assemblies [36FF], and the flow of aerosols released in postulated nuclear accidents [34FF] have been described.

## 10. Rotating surfaces

### 10.1. Rotating disks

Two numerical studies were performed on the flow between rotating disks. In the first [1G] the two disks rotate with different time dependent velocities. In the second [3G], mixed convection is studied with co-rotating and counter rotating disks with and without a shroud. The fluctuation of rotation power was measured for two counter rotating disks with and without a shroud [2G]. The sliding interface between a stationary pin and a single disk was studied theoretically [5G]. A rotating cavity with axial throughflow was used to model a compressor drum cavity [4G].

### 10.2. Rotating channels

Several numerical [15G,12G,8G,6G] and experimental [14G] papers describe flow and heat transfer in channels rotating about an axis perpendicular to the

channel axis. A description of a new research facility was also given [18G]. Additional studies considered curved channels [10G,20G] and channels with ribs [9G,19G]. Experiments were performed for flow in a pipe rotating about its axis [11G] and numerical solutions were obtained for flow in rectangular and elliptical ducts rotating about a parallel axis [16G]. The performance of an annular heat exchanger with the inner cylinder rotating [21G], rotating annuli [7G], and the flow in the annulus around a rotating cylinder [13G] were reported. Heat transfer to liquid helium in a high speed rotating field was investigated [17G].

### 10.3. Enclosures

Geometries considered in rotating enclosure flows include a rotating cylinder [29G] and an annulus [24G]. Studies of rotating liquid layers include development of criteria for the onset of Benard–Marangoni convection [28G] and the transition to turbulence for Rayleigh–Benard convection [25G]. Numerical and experimental studies were made on convection in a differentially heated cubic cavity rotating about its center [26G,27G]. Theoretical solutions have been obtained for flow in a spherical annulus [22G] and from a rotating cylinder contained in a rectangular enclosure [23G].

### 10.4. Cylinders, spheres, bodies of revolution

Heat transfer by forced [31G] and mixed [33G] convection from rotating cylinders has been predicted. Forced [34G] and mixed [30G] convection from rotating spheres has also been investigated. The effect of aspect ratio was determined for heat transfer from a rotating cup [32G].

### 10.5. Miscellaneous

A theoretical investigation was performed on the transient dynamics and heating of a droplet in a gas flow [37G,38G]. The effects of rotation on ice formation [35G] and on spacecraft boom deformation [36G] were studied.

## 11. Combined heat and mass transfer

The present section on combined heat and mass transfer covers a number of important cooling mechanisms. These include transpiration cooling, ablation, film cooling, jet impingement heat transfer, spray and mist cooling and drying systems.

### 11.1. Transpiration and ablation

A transpiration coolant passes through a porous surface to protect the surface from a hot gas stream flowing over it, while ablation occurs when a high heat flux to a solid surface produces loss of material by a number of processes including sublimation and chemical decomposition with the intent of absorbing the heat transferred from a high velocity and temperature flow to prevent damage of the structural surface underneath the ablating material. Two dimensional axisymmetric ablation problems have been analyzed using an unstructured grid to include the effective change of surface shape [3H]. Change of shape of an ablating solid and the transient temperature distribution inside it has been analyzed with a three-dimensional conduction model [4H]. The effect of mechanical erosion on an ablating carbon-base material has been examined [5H]. The ablation of a cellulosic cylinder degrading from high pressure contact against a hot, spinning disc has been analyzed [2H]. Transpiration cooling studies include an analytical model for air injection from a hemicylinder [6H], transpiration with turbulent flow over a two dimensional contoured nozzle [1H] and the use of a perforated plate with different hole sizes for the transpiring holes [7H].

### 11.2. Film cooling

With film cooling, fluid is injected at discrete locations along the surface into the boundary layer to prevent overheating of a wall from exposure to a high temperature fluid. Film cooling from a row of holes along a turbine blade has been studied in a cascade at different free stream turbulence levels [10H] while a three-dimensional code has been used to study the effect of spanwise pitch of shower-head holes at the leading edge of a turbine blade [8H]. Film cooling performance for injection through discrete holes in the endwall of a turbine blade is investigated [9H]. The effect of bulk flow pulsations on the injection [15H] and the film cooling performance [16H] have been studied with single-row film cooling along a surface. Film cooling in a duct has been examined for both subsonic and supersonic flow [13H]. Another analysis considers different angles of film cooling holes taking their flow from a duct at different velocity ratios [14H]. Film cooling with a supersonic flow at Mach 2.35 has been examined experimentally [12H]. Other film cooling studies include applications to protect electronic modules [11H] and injection into a flow over a rearward facing step [17H]. A computation shows some significant physical influences in a film-cooled high-speed nozzle flow [18H].

### 11.3. Submerged jets

The thin boundary layer in the stagnation region of an impinging jet provides high localized heat transfer while an array of jets can cool larger surfaces. Submerged jets are jets in which the fluid in the jet is similar to the fluid in the surroundings. Studies on heat transfer of impinging jets include measurements with differential thermocouple heat flux sensors [45H], the influence of the turbulent statistics in the stagnation region on heat transfer [40H], and the effect of shear layer dynamics on local and average heat transfer [38H]. The instabilities in a supersonic impinging jet [26H] and the effect of turbulence on heat transfer in stagnation flow [19H] have been reported. Jet impingement has been used to dry a moist, porous solid [25H] and to heat a phase change material [21H]. Jets impinging on a surface in a confined geometry have been studied including the influence of nozzle geometry [22H], and turbulence intensity [36H]. A  $k$ - $\epsilon$  turbulence model has been used to predict heat transfer to a fully developed turbulent axisymmetric jet within a semi-confined space [20H]. Liquid crystals have been used to study the heat transfer from a pair of impinging air jets [46H] while a numerical investigation provides information on heat transfer with rows of impinging jets [32H]. The effect of fluctuating velocity on impingement heat transfer with an excited circular jet [37H] and a self-oscillating jet [41H] have been reported. Use of a self-oscillating jet has also been examined for drying applications [43H]. Flow and heat transfer has been studied from an impinging torch using an interferometer and stroboscopic photography [29H]. Jet impingement has been used to prevent overheating of cutting tools in manufacturing [33H, 34H] and for continuous annealing in steel strip manufacturing [39H]. Particle image velocimetry and laser-induced fluorescence have been used to examine the flow and heat transfer of an excited plane impinging jet [42H] while supersonic impinging jets have been examined to show the influence of shock–vortex interaction [24H].

Laminar wall jets on plane and cylindrical surfaces have been studied, including the influence of suction and blowing on heat transfer [44H]. Experiments on a plane wall jet include the use of a thermochromic liquid crystal to measure temperature distribution [30H] and hot-wire anemometry to study the flow characteristics [31H]. A two dimensional analysis has extended the solution for a wall jet to show potential instabilities [35H]. Experiments have been reported on interaction of two turbulent curved wall jets [27H]. Other studies have been reported on the analysis of mass transfer to a wall jet with chemical reaction at the fluid–solid interface of [23H] and heat transfer to a buoyant ceiling jet [28H].

### 11.4. Liquid jets and sprays

Individual liquid jets and sprays from liquid jets are used in a variety of cooling applications. Studies on heat transfer to liquid impinging jets include the influence of nozzle diameter on local heat transfer [47H] and the cooling of an array of heated strips from an impinging fluorinert coolant [49H]. Numerical analysis is compared to an approximate solution for determining the heat transfer from a two-dimensional vertical liquid jet against a hot, horizontal plate [50H]. Applications of spray cooling to steel production [52H] and desalination systems [51H] have been reported. An air/liquid mist created in jet atomizer has been used to cool heated surfaces [48H].

### 11.5. Drying

Combined heat and mass transfer under drying conditions has been examined in a number of basic and applied systems. Models predict heating and drying with internal energy dissipation such as in microwave heating [54H], direct contact rotary drying [62H], particulate solid drying with a neural network model [56H] and drying of droplets containing dissolved biomass [59H]. Experiments on drying systems include the use of air and superheated steam as drying media [63H] and laboratory simulations of impulse drying with ceramic and steel plates [61H]. A number of applications to drying food have been modeled. These include sliding bed dryers for grain [60H], a model for drying wheat in a fixed bed [57H,58H], and drying systems for different foods [53H]. An analysis considers the drying potential of humid air [64H]. An optimization system for timber drying has been presented [55H].

### 11.6. Miscellaneous

Combined heat and mass transfer in wavy flowing films has been analyzed [77H] and studied in experimental systems [79H]. Studies of heat and mass transfer in tubes include evaporation effects of binary mixtures of refrigerants [69H] and mixtures of lubricating oil and refrigerants [68H]. Investigations describe heat and mass transfer with saline water flow in a cavity [76H] and the performance of a spined-tube absorber [71H]. Analyses have been performed for heat and mass transfer during nonisothermal gas absorption in a two-phase gas–liquid mixture [73H], for transport through inert liquids [72H], and for dehumidification of the air in lithium chloride solutions in a packed column [70H]. Combined heat and mass transfers through solid matrixes has been examined for a three layer building envelope and a single and multi-layer fabric

systems [67H]. Heat and mass transfer analyses have considered flows in soils [78H], clay buffers [80H] and the adsorption of water on zeolite [74H]. Other studies include processes involving bulk refrigeration of fruits and vegetables [66H], modeling of single drops in liquid-liquid mixtures [75H] and hydrogen and thermal transport in laser beam welding [65H].

## 12. Change of phase — boiling

Thermal transport phenomena associated with liquid-to-vapor phase change are addressed in the publications reviewed in this section and classified into four major categories: droplet and film evaporation (19 papers), bubble characteristics and boiling incipience (17 papers), pool boiling (40) and flow boiling (47). In addition to these papers, dealing with evaporative and ebullient heat transfer, the interested reader will find these phenomena addressed in some of the papers included in the following sections: change of phase  $\tilde{n}$  condensation (JJ), heat transfer applications  $\tilde{n}$  heat pipes and heat exchangers ( $Q$ ), and heat transfer applications  $\tilde{n}$  general (S).

### 12.1. Droplets and film evaporation

The 1996 archival literature presents several fundamental studies of evaporation from a single droplet, including the application of perturbation theory to the prediction of evaporation and combustion rates [6J], the modeling of flash evaporation from a droplet exposed to a high-speed air stream [7J], and the use of holographic techniques to obtain the radial distribution of evaporated diffusing vapor [18J]. The evaporation rates and onset of instability in the EHD-enhancement of droplet evaporation are discussed in [16J,17J] respectively.

The fluid mechanics of droplet impaction on flat walls underpins models of diesel combustion and spray cooling and is explored in [4J,15J] — describing the incorporation of droplet impingement models into numerical codes for combustion in an internal combustion engine, [3J] — addressing an anomalous region in the boiling curve for jet mist cooling, [11J] — focusing on the effect of droplet sensible heat on the cooling rates, [12J] — comparing computer predictions with anemometry data for droplet velocity and size in the wall spray, [5J] — comparing theoretical predictions with experimental data for spreading ratios and times of impinging droplets, [2J] — describing the influence of large surface roughness on droplet impact and spreading, and [14J] — presenting photographic data and fast response thermocouple measurements during droplet impact in low gravity.

Recent studies of evaporating liquid films have addressed important aspects encountered in actual engineering applications. The microscopic details of fluid flow and heat transfer near the contact line of a curved evaporating liquid film are, thus, examined in [8J], nonequilibrium evaporation of a heated film in microgravity in [9J], the effect of longitudinal fins on evaporation of falling films on horizontal tubes in [13J] as well as the enhancement associated with the use of thin glass rods to disturb the liquid film in [19J], and the changes caused by the presence of lubricant on the evaporative heat transfer performance of refrigerants R-134a and R-22 in [10J]. A procedure for selecting the optimum number of effects for evaporators used in chemical process plants is proposed in [1J].

### 12.2. Bubble characteristics and boiling incipience

[20J] uses a variational form of mechanical energy conservation, in both the liquid and the vapor, to derive the characteristics of a bubble growing at a nucleation site on a horizontal wall. [21J] develops a nonequilibrium relaxation model for one-dimensional flashing liquid flow. The effects of microgravity on the growth rates of hemispherical bubbles are studied and theoretically-bounded in [24J], the effects of elastic viscosity and diffusion resistance on the growth of vapor bubbles in a superheated polymer solution are the subject of [32J,25J]. In [31J] the growth of vapor bubbles within a porous medium was studied both experimentally and theoretically. A new dynamic instability, associated with the onset of boiling in a single-channel, high-pressure upflow was described in [35J].

Digitally-enhanced measurement techniques were used in several studies to examine the characteristics of bubbles encountered in vertical bubbly flow, including [34J] — in which an electroresistivity probe was used to obtain phase-resolved temperatures, as well as volume fraction, bubble frequency, and bubble velocity for air–water and air–multifluor flows [36J] — in which high-speed photography and digital image processing techniques were applied to the determination of bubble properties encountered in subcooled flow boiling, and [29J] — in which decentralized processing of multiple fiber-optic sensors was used to map the local void fraction and bubble properties for an air–water flow.

While the homogeneous nucleation kinetics near a small evaporating drop were investigated in [23J], [33J] describes the results of experiments involving laser-induced bubble formation in liquid nitrogen and [22J] the results for the onset of nucleate boiling and of critical heat flux for liquid nitrogen on substrates of differing roughness. The transition to boiling, as well as other transient phenomena, of He II in a vertical

channel [28J], of liquid 3He and mixtures of 3He and 4He below 1 K [27J], and of liquid nitrogen and helium under rapidly increasing heat fluxes [30J] are also described. [26J] present evidence of suppression of the incipience hysteresis in highly-wetting liquids, through the use of micrographite fiber nucleation activators.

### 12.3. Pool boiling

Fundamental studies of pool boiling heat transfer, published during 1996, described the development of a new additive model for bubble-induced heat transfer [39J], experimental results for nucleate boiling of binary mixtures [51J,52J,59J], experimental data for pool boiling in microgravity [66J], boiling of HeII under steady and transient conditions [69J], and the influence of surface properties on transient pool boiling [46J]. Nontraditional experimental techniques were employed by several investigators to elucidate pool boiling behavior, including the use of temperature controlled surfaces to obtain precise boiling data [41J, 47J], use of liquid crystals thermography to map the variations in wall superheat [60J], and laser-Doppler anemometry to determine the contribution of each of four heat transfer mechanisms to ebullient thermal transport [38J].

The influence of heater geometry on pool boiling was examined in [48J] — which provides a review of the literature dealing with pool boiling from inclined and downward-facing smooth plates, in [55J] — which discusses the heat transfer mechanism for boiling on the outside of horizontal tube bundles, in [44J] — which presents the results for boiling on various combinations of tube diameters, surface roughness, and tube orientation, in [56J] — wherein the effect of plate orientation and surface treatment on pool boiling of He is explored, and in [75J] — which deals with boiling from a rotating disk.

The 1996 literature is rich in studies of pool boiling enhancement. A review of the many techniques developed to improve ebullient and convective thermal transport is offered in [40J]. Boiling heat transfer from porous metal and metal mesh surfaces is described in [45J,63J,71J]. The effect of an anionic surfactant on the pool boiling of water is examined in [37J]. Ebullient heat transfer from finned surfaces is the subject of [54J,61J], while boiling in vertical channels is examined in [72J]. The beneficial effect of electric fields on pool boiling from smooth plates is the subject of [43J,67J], while [65J,74J,73J] deal with the influence of an EHD field on pool boiling from a passively-enhanced surface.

The instabilities induced during the transition from nucleate to film boiling were studied analytically in

[53J,42J]. Pool boiling CHF in liquid metals, including data and new correlations, was surveyed in [68J] and the onset of stable film boiling was the subject of [64J]. Film boiling on a downward-facing curved surface was explored in [49J], while the influence of dissolved gas on film boiling in water and of mass diffusion on film boiling in binary mixtures were investigated in [58J,62J], respectively. The role played by pool boiling in the grinding process is described in [76J,57J], in the preparation of grease in [50J], and in the cooling of electronics, through the use of a thermosyphon, in [70J].

### 12.4. Flow boiling

The growing interest in new refrigerants and ongoing research on the cooling of fusion reactors are largely responsible for sustaining the flow boiling literature during this past year. A new hypothesis of thermodynamic states was used to underpin an analytically-derived flow boiling curve [108J]. New experimental studies revealed that in annular flow the forced convection mechanism dominates over secondary nucleation in the liquid film [111J]. The characterization of local flow boiling heat transfer coefficients under very high heat flux conditions revealed a need for major modifications in correlations used to describe the subcooled partial nucleate boiling domain [78J]. Flow boiling under reduced gravity conditions was the subject of [87J] — examining annular gas–liquid mixtures, and [118J] — focusing on verification of the “sliding bubble” mechanism with high subcooling. Studies of flow boiling heat transfer rates in unconventional fluids, including organic–water solutions [122J] and electrolyte solutions [101J], as well as in unconventional geometries, such as porous media [114J], narrow channels [96J], microchanneled plates with binary mixtures [105J], during loss-of-coolant reactor scenarios [103J], and swirl tubes [76J,109J] are described in the 1996 archival literature.

Ebullient heat transfer to refrigerants received considerable attention in the 1996 literature. A state-of-the-art review of refrigerant boiling was presented by [112J]. Flow boiling heat transfer coefficients for R-134 and R-12 flowing in microfin tubes [110J] and in small circular and rectangular channels [115J], respectively, R22 and R407C (itself a mixture) flowing in a microfin tube [95J], both boiling and condensation of quaternary refrigerant mixtures [107J], and the flow boiling behavior of ammonia [104J] have also been reported. The EHD enhancement of flow boiling heat transfer for R-134a flowing in a tube bundle and R-404a in a microfin tube is described in [80J] and [106J], respectively, while the mechanism by which helical ribbing enhances two-phase heat transfer was examined in



[120J]. Experimental techniques for establishing the flow parameters of importance in two-phase heat transfer are discussed in [97J] — dealing with the use of a steady or pulsed neutron beam, in [93J] — dealing with the use of a nonintuitive auto-transformer technique, and [90J] — dealing with the application of laser holography to shock wave propagation and onset of boiling in He II.

Modeling of the “boiling crisis” in flow boiling continues to receive significant attention. Recent publications explored various geometric effects, including the influence of tube diameter on CHF in subcooled flow boiling in [79J], the contribution of spacers and mixing vanes on low velocity CHF in water [81J], and the impact of twisted-tape inserts on CHF in subcooled, small diameter tube flow [113J]. The effect of nonuniform heating [102J], of subcooling and velocity [89J], countercurrent annular flow in a thermosyphon [98J], and oscillatory flow conditions [116J,100J] on flow boiling CHF have also been described. Electronic cooling applications, constrained by the boiling crisis, and applications in which CHF thermal modeling capability must be linked to thermal stress computations, are discussed in [86J,119J] respectively.

Post-CHF and post-dryout phenomena in flow boiling systems are explored in [83J] for one-sided heating and high subcooling and in [91J] for low flow conditions. [88J] examines subcooled film boiling of refrigerants in upflow, while [117J] presents the results of an experimental study of dispersed flow heat transfer in circular bends.

Spray and jet impingement cooling constitute a special case of flow boiling behavior and provide a fertile field for heat transfer research. The transition from jet-induced convection to nucleate boiling is studied experimentally in [84J,85J]. The fundamental issues encountered in the boiling of a free-surface, planar jet are the subject of [121J], the interaction between a liquid spray and subcooled liquid film is examined in [94J] and the self-similarity of heat transfer to jets in a multiple jet array is described in [99J]. The application of two-phase multiple jet impingement to the cooling of electronic equipment is discussed in [82J,92J].

### 13. Change of phase — condensation

Papers on condensation during 1996 were separated into those which dealt with surface geometry effects, those on the effects of global geometry and thermal boundary conditions, papers presenting techniques for modeling and analysis, papers on free-surface condensation, presentations of unsteady effects, and papers dealing with binary mixtures.

#### 13.1. Surface geometry and material effects

One paper analyzed the thermal interaction between laminar film condensation, forced convection, and a conducting wall separating the two [4JJ]. Several dealt with tubes, one with low-fin and 3-D fin enhancement [3JJ], a second with 3-D fins [5JJ] and a third with microfins [2JJ]. Finally, an analysis was performed with plates on which there is fog formation [1JJ].

#### 13.2. Global geometry and thermal boundary condition effects

The bulk of the activity in 1996 was in this category. A numerical solution showed the effects of taking fin nonisothermness into account [24JJ], another conjugate analysis discussed the effects of finite thermal inertia on the problem of condensation on a vertical plate [28JJ], while another analyzed the heat, air, and moisture transport in a residential wall [20JJ]. Several papers investigated tube geometries. One presented a theory for condensation in a vertical tube [19JJ], another presented a measurement technique for experimentally determining the in-tube condensation heat flux [16JJ], while another applied the population balance model to analyze condensation inside of a horizontal tube [9JJ]. An analysis was presented for nonisothermal absorption on horizontal tubes used in absorption heat pump applications [10JJ], another used numerical methods to deal with noncondensables in horizontal tubes and tube banks [7JJ], while another looked at the effects of condensation inundation and noncondensable gases in horizontal tube bundles [33JJ]. Several focused on fin enhancement. One presented a review of properties of refrigerants for low-finned tube applications [27JJ], another presented experimental results for horizontal integral-finned tubes [11JJ], another similar paper focused on low-thermal conductivity fins [14JJ], and another concentrated on R-123 applications [26JJ]. Condensation in tubes of small hydraulic diameter was experimentally evaluated [30JJ,31JJ], condensation was seen to be a limiting process in the cooling of fibers with cross-flow [25JJ], and moisture conditions were addressed for walls with cellulose, loose-fill insulation construction [13JJ]. Three papers dealt with greenhouses; two on dynamic heat transfer [22JJ,23JJ] and another on the influences of condensation and rain on heat transfer coefficients of claddings [21JJ]. Two papers were on nuclear plant containment vessels, one discussed comparisons between computations and test data [15JJ] and another presented primary parameters and methods for heat transfer coefficient evaluation [12JJ]. Other geometric features studied include steam turbines [6JJ], rotating disks [32JJ], agitated vessels [17JJ], closed thermosyphons [18JJ], and cryogenic

traps [8JJ]. Finally, experimental results were presented for augmentation of condensation by electrohydrodynamical means [29JJ].

### 13.3. Modeling and analysis techniques

Papers which seemed to focus on analysis techniques included two which accounted for the effects of wall conduction [41JJ,37JJ], two which showed numerical modeling of condensation with noncondensable gases [39JJ,40JJ], another focused on nonequilibrium condensation in a hypersonic flow [38JJ], and one near-critical region characteristics [35JJ]. Papers dealt with on system analysis included one on inverted U-tubes [34JJ] and another on fume formation and deposition in kraft recovery boilers [36JJ].

### 13.4. Free surface condensation

Free surface condensation papers were on surface wave effects [46JJ, 45JJ] and on desorption of carbon dioxide from falling films [42JJ]. A two-paper presentation dealt with condensation on water drops [47JJ,44JJ], while another discussed condensation with hygroscopic aerosols [43JJ]. A dropwise condensation paper investigated the performance of Langmuir–Blodgett surfaces [48JJ].

### 13.5. Unsteady effects

Condensation papers were presented for pulsating bubbles [52JJ], translatory motion of bubbles with high Nusselt numbers where the unsteadiness comes for their rapid growth [49JJ], and condensation influenced by sound [51JJ]. Instability considerations were directed to film growth on a vertical surface [50JJ] and homogeneous nucleation in a laminar flow reactor [53JJ].

### 13.6. Binary mixtures

Studies with binary mixtures were in vertical tubes [55JJ] and channels [58JJ], horizontal tubes [54JJ], and with noncondensable gases [56JJ]. Finally, a paper was presented for pseudo-dropwise condensation in a binary mixture [57JJ].

## 14. Change of phase — freezing and melting

### 14.1. Melting and freezing of spheres, cylinders and slabs

Several freezing investigations in cylindrical and slab

geometry were performed. Among the cylindrical geometry studies was ice film accretion on a rotating cylinder to simulate marine conditions [4JM]; melting characteristics along a bundle of horizontal heated cylinders [5JM]; experimental study of natural convection melting of a horizontal ice cylinder immersed in immiscible liquid [oil] [6JM]; and exothermic heat of mixing measured during melting of ice cylinders in sulfuric acid [3JM]. Slab geometry's were investigated in polymer freezing for crystallinity and spherulite effects in reinforced carbon fiber matrix [1JM], and an exact solution of freezing during deep-freezing of slab products was developed [2JM].

### 14.2. Stefan problems

Fikiin [7JM] developed a generalized numerical modeling for a Stefan problem using an improved enthalpy approach based on a quasi-one-dimensional formulation.

### 14.3. Ice formation/melting in porous materials

Studies in this area included investigations into natural convection melting of porous media in a rectangular enclosure [8JM]; principles of ice formation in biological materials for cryopreservation [10JM]; experimental and theoretical prediction of freezing times of strawberry pulp in large containers [11JM]; numerical modeling of snowmelt infiltration into frozen soil [12JM]; modeling of melting in heterogeneous snow cover on permeable frozen soil [13JM]; and a numerical analysis of rectangular foods during freezing [9JM].

### 14.4. Contact melting

One study, [14JM], established a heat transfer correlation for natural convection in a cavity for contact melting applications.

### 14.5. Melting and melt flows

Activity in this area fell into several major groupings: injection molding, laser melting, metal melts, and miscellaneous.

Injection molding studies investigated microflow marks as a function of the melt temperature in injection molding [38JM]; experimental and numerical study of polymer melt growth in an injection molded part [21JM]; calculation of cooling time in injection cooling [26JM]; and the use of BEM modeling to analyze complex 3D geometric problems in injection molding [30JM].

Thermal effects in pulsed laser melting was studied by [17JM] and a kinetic theory for laser pulse heating

including heat transfer in the melt was presented by [32JM]. Other modeling work investigated: laser cutting using BEM [24JM]; heating and melting during pulsed laser fabrication of ultra-shallow  $p$  plus-junctions at the nanoscale [39JM]; non equilibrium temperature field around the melting and crystallization front induced by pulsed laser irradiation [33JM]; and numerical predictions of oscillatory flow convection in a laser melt pool [29JM]. Experimental studies of laser melting of Ti–15Al–20Nb alloy [37JM], and laser melting interface shapes in float zones [23JM] were also presented.

Experimental studies explored the use of microwave heating as a method to improve iron ore reduction [40JM] and a development of an electromagnetic levitation melting device [16JM]. Several other investigators studied various conditions in the melt: convection in liquid metals [15JM]; heat transfer in the siro-smelting process [34JM]; melt analysis due to electron beams in refining processes [28JM]; micropyrelic reaction in the melt [35JM]; simulation of thermosolutal convection in liquid metals [18JM]; numerical study of natural convection melting of pure metals in a cavity [31JM]; Marangoni convection in a 1D model of float zone in a melt [27JM]; and simulation of heat and fluid flow and interface shapes in float zone of lithium niobate melt [20JM]. In addition, modeling of nonisothermal melt flows with water [22JM] and a numerical study of melt–water interaction [25JM] were presented.

Cyclic phase change [freezing and melting] with fluid flow was studied by [36JM] and the viscous stagnation flow solidification problem for a pure substance was addressed by [19JM].

#### 14.6. Powders, films, emulsions, and particles in a melt

The principles of ultrasonic wave atomization of a viscous melt was described by [41JM].

#### 14.7. Glass melting and formation

Several glass burners were described including the cleanfire High Radiation burner which maximizes heat transfer [42JM], and a submerged combustion furnace [46JM]. Analysis of heat transfer optimization in oxy-fuel burners [44JM] and an analytical model to evaluate particulate emissions in oxy-fuel fired glass furnaces [45JM] was also presented. Lastly, [43JM] developed a numerical simulation of creeping flow and heat transfer in a forehearth for glass bottle production.

#### 14.8. Welding

A review of heat transfer studies in arc welding was

presented by [49JM]. In addition, studies on thermal cycles in multiple electrode submerged arc welding [47JM] and measurement and prediction of energy absorption in laser beam welding [48JM] were performed.

#### 14.9. Enclosures

An experimental enclosure phase change study was performed using paraffin materials [51JM]. In addition, numerical studies with multizone adaptive grid generation in several enclosures including rectangular, eccentric annuli, and an open cavity [52JM] and a study of flow in and heat transfer across a vertical cavity of water during freezing [50JM] were performed.

#### 14.10. Nuclear reactors

High pressure melt ejection and corium dispersion was studied in large scale models [53JM], in scaled experiments and models by [54JM] and [57JM], and in a scaled annular cavity [55JM]. In addition melt flow dispersion of direct containment heating of a nuclear reactor [58JM] and the molten pool thermal hydraulics during molten core–concrete interactions in a nuclear accident were investigated [56JM].

#### 14.11. Energy storage

Energy storage by PCMs were studied by various groups. Their studies included: measurement of heat transfer characteristics in low-temperature PCM systems using salt-hydrates [60JM]; latent heat thermal energy storage enhancement by using an externally finned [73JM] and an internally finned radial tube [74JM]; thermal storage in a hollow cylinder of PCM [75JM]; and PCMs for use in thermal control of plastic quad flat packages [69JM]. In addition several numerical studies were performed to study thermal protection by latent heat absorption of a PCM filled rectangular cell [66JM,67JM]; cold heat release of PCM of air-emulsions for direct-contact heat exchange [68JM]; cooling of a heated surface with PCM [70JM]; enhanced heat transfer by insertion of a metal matrix into PCM [71JM]; and thermal radiation effects in PCM systems [72JM].

#### 14.12. Multiple PCM studies

The superiority of mixed PCM families vs. single PCM families for energy storage was studied by [59JM]. Other studies in this area included: cyclic heat transfer in a novel storage unit of multiple PCMs [61JM]; 1D FEM model for enhancement of energy charge–discharge rates in slabs of different PCMs

[62JM]; FEM study of multistage PCM system [63JM]; exergetic study of energy storage using multiple PCMs [64JM]; and a theoretical study of thermal energy storage by PCM [65JM].

#### 14.13. Mushy zone—dendritic growth

Work in this area included a study to improve the enthalpy method for multicomponent phase change conditions [78JM]. Other work investigated oscillatory instability during binary alloy solidification in the mushy layer [76JM] and thermosolutal convection during freezing of seawater [77JM].

#### 14.14. Metal solidification

Studies of metal solidification included work in binary alloys and other metals.

Binary alloys studies included: modeling of macroscopic heat flow with microscopic nucleation and growth in a binary alloy [80JM]; numerical study of the solidification of a binary alloy with globulitic morphology [79JM]; study of instabilities in fluid layer of a binary alloy during freezing [83JM]; scaling analysis of unidirectional solidification of a binary alloy [84JM]; modeling of directional solidification to test stability in lead/tin system with remote flow [82JM]; theoretical study of the formation of island films from binary melts [85JM]; and a numerical study of heat and fluid flow in directional crystal growth of GaAs [87JM]. In addition, studies on the heat transfer in spray formed billets [81JM] and numerical approaches to solidification [86JM] were presented.

#### 14.15. Crystal growth from melt

Work in this area was broken up into Czochralski, Bridgman and general crystal growth topic areas.

Czochralski crystal growth was simulated by [89JM] and a numerical study of Czochralski melt configuration was presented by [102JM]. In addition, a numerical and experimental study of oxygen transfer during Czochralski growth of a single silicon crystal in a magnetic field [94JM] and an experimental study of Czochralski growth of BGO and BSO crystals [105JM] were presented.

Bridgman crystal growth was investigated experimentally to assess interface curvature in vertical Bridgman growth of InP crystals [104JM] and gravity induced heat transfer effects during Bridgman growth of InGaAs [90JM]. Numerical simulation of Bridgman growth was also used to investigate the following: interface curvature and macro-segregation in vertical Bridgman growth [93JM]; optimal design strategy for Bridgman crystallization process [91JM]; heat and

species transport in vertical Bridgman crystallization processes [92JM]; liquid encapsulated vertical Bridgman crystal growth [98JM]; and Bridgman growth of beta-NiAl crystals [101JM].

A review of crystal growth work at Fukuda Laboratory in Japan over the last 25 years was presented by [103JM]. In addition, general crystal growth topics covered included: latent heat effects on crystal interface stability [96JM]; study of interface shapes and thermal fields during gradient solidification of single sapphire crystals [88JM]; analysis of radiative heat transfer in crystal pulling [95JM]; numerical study of the use of magnetic fields to radially segregate dopants in silicon crystal growth [97JM]; numerical study of crystal growth in vertical zone melts [99JM]; and the study of kinetics and size of crystals formed for use in purification of food concentrates [100JM].

#### 14.16. Casting

The principles of a new technique of “microcasting” of steel objects was investigated by numerical and experimental study of the interface heat transfer and bonding characteristics of successively impinging molten metal droplets [106JM].

#### 14.17. Splat cooling

Experimental investigation of molten solidification on a substrate for use in splat cooling applications was presented by [107JM].

#### 14.18. Miscellaneous

Several miscellaneous phase change studies were also presented. These included: experimental-numerical prediction of thermal properties during phase change [108JM]; a 1-D numerical model of ice formation and melting on lakes [109JM]; and an experimental study of natural convective freezing of warm water faster than cold water under some circumstances [110JM].

### 15. Radiative heat transfer

The papers below are divided into subcategories which focus on the different impacts of radiation. Papers describing the development or application of models dominate the literature on radiative heat transfer. Papers focusing on the numerical methods themselves are reviewed in the numerical methods section under subcategory radiation.

### 15.1. Influence of geometry

The calculation of view factors for different geometries continues to be of interest. Analytic expressions for concentric-cylindric view factors are given in [7K]. Khoddam et al. [2K] derive a view factor for a nonuniform cross-section shaft and a concentric cylinder. A cell-to-cell transport Monte Carlo method was developed by Palmer et al. [6K] and applied to arrays of fixed discrete surfaces. Antoniak et al. [1K] address the same problem with the MCLITE code. The radiative exchange between square parallel channels in a concentric monolith structure is modeled in [8K]. A finite volume method for radiative heat transfer in cylindrical enclosures is presented by Moder et al. [5K]. Axisymmetric radiation transfer through cylinders as well as nonaxisymmetric transport through two- and three-dimensional sectors is considered. The radiative heat transfer in three-dimensional complex geometries using the Discrete Transfer Method is described in [3K]. The method is based on body-fitted grids so that it can easily be used in CFD calculations. The reduction of the radiative load on cryostats windows by straight and bend tubes is studied in [4K]. Papers discussing enclosures and processing chambers are referenced in the section on radiation combined with convection and conduction.

### 15.2. Participating media

Papers in this category can be divided into those which focus on emission and absorption of the media and those which deal with scattering.

Radiation transfer in molecular gases such as CO<sub>2</sub> [22K] and O<sub>2</sub> [32K] is discussed. Lallemand and Webber [27K] use an exponential wide band model to determine radiative properties of a variety of molecular gases. The model for rotary desorbers of Cook et al. [17K] takes into account the real nature of the participating gas as well as CO<sub>2</sub> and H<sub>2</sub>O in the gas phase. Bhattacharjee et al. study the influence of gas-phase radiation from O<sub>2</sub>:N<sub>2</sub> mixtures in flame spread in microgravity [13K]. Strong radiation solely from three-atomic molecules characterizes combustion using synthetic air [33K]. Radiative transfer in nongray gases is considered in [16K,24K,38K]. A procedure for reordering absorption coefficients to predict radiative gaseous exchange is proposed by [28K]. Bressloff et al. [15K] assess the performance of a differential total absorptivity solution of the radiative transfer equation. Kamiuto et al. study combined radiation and convection in absorbing and emitting gases [23K]. Radiation from shock wave heated gases was studied in a number of investigations: air was considered in [29K,12K,40K,47K], the effect of argon additions to

N<sub>2</sub>-CH<sub>4</sub> is pointed out in [26K]. Shock tube experiment were conducted in a simulated atmosphere of Titan in order to study the simulated shock layer of the Huygens probe, which will enter the Titan atmosphere in 2003 [37K].

The emission and absorption of radiation by particulates plays an important role in high soot density flames [9K,25K]. Baek [11K] studies the ignition of propane-air mixtures by radiatively heated inert particles.

A large number of studies deal with the effects of scattering and/or refraction. A two flux method has been used to model the radiative transfer in semitransparent layers [44K,45K,42K] and in composites [43K,46K]. Scattering also plays a major role for the radiative transfer in porous media [20K,10K], powdered and fibrous polymers [36K], as well as fibrous thermal insulation [18K,19K,34K]. Siegel [41K] discusses internal radiation effects in zirconia thermal barrier coatings. Dependent/Independent scattering regimes were studied in [21K] using a discrete dipole approximation.

The radiative transfer in two-layer media with Fresnel interfaces is analyzed in [48K,30K]. These studies are extended to multi-layer media in [31K]. Absorption, emission and scattering in two-dimensional media is investigated in [49K,39K,14K]. Combined effects of radiative and conductive heat transfer can lead to thermal stresses in semitransparent sapphire crystals which is discussed in [35K].

### 15.3. Radiation combined with convection, conduction, or mass transfer

The interaction between conduction, convection and radiation was studied in such different investigations as on rapid thermal processing systems [72K], gradually expanding channels [67K], discretely heated open cavities [54K], L corners [51K], backward facing steps [68K], packed beds [64K], and isobutane crackers [53K]. Radiation and conduction heat transfer play an important role in silica aerogels [61K]. Coupled inverse conduction-radiation problems are considered in [78K]. The authors propose an iterative algorithm based on a space-marching technique. Sakami et al. [79K] use a discrete ordinates method to describe the conductive-radiative heat transfer in complex two-dimensional geometry. A finite-volume multi-grid solver is proposed in [65K] for the modeling of gray-body surface radiation coupled with fluid flow. A finite volume method is also used to describe the radiative-convective heat transfer around a circular cylinder in a cross flow [70K]. Convection and radiation also play a role in thermocapillary flows in microgravity [66K] and in chemically reactive nozzle flows [71K,75K]. Convection

and radiation in micropolar fluids is studied in [77K]. Convection and radiation interaction are also important in fluidized beds [56K], in porous radiant burners [69K], in the transient thermal performance of line traps [60K], in waste-heat boilers [82K], and in furnaces [59K,76K,63K]. Natural and mixed convection combined with radiation are considered in [80K,62K,50K] and in the discussion of enclosures [73K,52K]. Combined heat transfer is also discussed in connection with insulation [57K,58K] and radiation barriers in ventilated attics [74K,81K]. Heat, momentum, and mass transfer are considered in the shrinking of biomass particles exposed to thermal radiation [55K].

#### 15.4. *Intensely irradiated materials*

This year only a small number of studies is concerned with intensely irradiated materials. Foss and Davis discuss the transient laser heating of single solid microspheres [83K] based on a Mie theory model. Ultrashort laser pulses are used for the heating of silicon microstructures in order to reduce adhesion [84K]. The use of CO<sub>2</sub>-laser radiation for the localized curing of epoxy-based materials is described by Scarparo et al. [85K].

#### 15.5. *Experimental methods and properties*

A number of studies focused primarily on experimental methods. Interference images were used to determine the temperature distribution in the boundary layer near the wall in studies of propagation of premixed flames in a closed vessel [87K]. A direct radiometric technique was used to measure the spectral and directional distribution of radiation exiting a packed bed [90K]. Jones et al. [89K] measure the spectral-directional emittance of oxidized copper in a wavelength range from 2–10 micron. Zaworski et al. [93K] use Monte-Carlo methods to interpret their measurements of bi-directional reflectance data. Spectral IR directional-hemispherical transmission and reflection measurements were performed in [86K] on fine cell PU rigid foams. The measurement of Hall coefficients and DC resistivities was used to determine radiative properties of liquid metal alloys [88K]. Yoshida et al. [92K] report the simultaneous measurement of thermophysical and radiative properties of semi-transparent liquids. The cooling characteristic of cutting grain in grinding is measured via infrared pyrometry using an optical fiber [91K].

## 16. Numerical methods

The development and application of numerical methods continue as topics of significant research. New procedures and algorithms are developed for solving the partial differential equations that govern heat transfer and fluid flow.

Methods are also adapted to new computer hardware enabling parallel processing. There is an ever-increasing variety of practical problems, to which numerical methods are applied. In this review, the papers that primarily focus on the application of a numerical method to a specific problem are included in the appropriate application category. The papers that describe the details of a numerical method are referenced in this section.

### 16.1. *General techniques*

New approaches and algorithms of general utility are described in a number of papers. A generalized object-oriented approach for solving differential equations is outlined in [2N]. The modified strongly implicit procedure is combined in [5N] with an adaptive optimization procedure based on the residual vector norm. The addition correction multigrid method is analyzed in [3N]. Reference [1N] describes different acceleration schemes for eigen function expansions of partial differential equations. Parallelization tools and their application to structured CFD codes are discussed in [4N]. Parallel computing is applied to heat and moisture transfer in unsaturated soils [6N,7N].

### 16.2. *Conduction*

The ADI method is extended to multidimensional heat conduction equation in [10N]. Transfer functions are used for obtaining transient temperature fields in cylinders [8N]. For diffusion models, [11N] describes a new boundary treatment as applied to hexagonal meshes. The conjugate heat and mass transfer is calculated in a desiccant system [9N].

### 16.3. *Buoyant convection*

Reference [15N] describes the analysis of the instability in buoyant convection in cylinders heated from below. The Galerkin and pseudo-spectral methods are compared in [12N] for the simulation of Rayleigh–Benard convection. Reference [14N] evaluates the roll patterns formed in a Rayleigh–Benard convection in a rectangular layer. The convection and solute segregation in vertical Bridgman crystal growth process are analyzed in [13N].

#### 16.4. Phase change

A temperature-based formulation is described in [16N] for the phase change situation. The Stefan problem in a stagnation flow is defined and investigated in [21N]. Reference [20N] develops a conjugate heat transfer analysis for a phase change system. Numerical anomalies in the simulation of directional solidification are discussed in [18N]. A finite-volume method is described for directional solidification [19N]. A number of numerical techniques are used to determine the effect of mold heat transfer during transfer molding [17N].

#### 16.5. Convection and diffusion

A new finite-volume method is described for the convection–diffusion problem [23N]. For high-resolution convective schemes, a novel technique is proposed for accelerating the convergence rate [22N]. Normalized splines are used for the finite-volume solution of convection–diffusion problems [25N]. Reference [24N] presents flux-based finite-volume formulations.

#### 16.6. Flow equations

A parallel implementation for solving the Navier–Stokes equations is described in [34N]. Reference [32N] develops a Fourier analysis of the SIMPLE algorithm on a collocated grid. A local grid refinement method for fluid flow analysis is described in [31N]. Reference [30N] reports on the performance of a multigrid method with a higher-order convection–diffusion scheme for three-dimensional flow. A simplified control-volume finite-element method is described in [29N]. Reference [26N] presents a complete pressure-correction algorithm for a nonstaggered grid. The continuity constraint method for three-dimensional fluid flow is given in [37N]. Time-dependent Navier–Stokes equations are solved by the vorticity–velocity method [36N]. A Riemann-problem-based approach is described for steady incompressible flows [35N]. Reference [33N] presents a second-order splitting algorithm for thermally-driven flows. Error estimation and adaptivity in finite-element analysis of convective heat transfer are discussed in [27N,28N].

#### 16.7. Application to special problems

A number of papers describe the application of numerical methods (with appropriate enhancements) to problems with special physical or numerical features. Reference [49N] presents a numerical study of flow and heat transfer in a wavy channel. Flow in an annu-

lus with a moving core is analyzed in [48N]. A multi-grid method is used to calculate thermocapillary convection [47N]. An analysis is presented in [46N] for the combustion chamber of a diesel engine. Reference [45N] describes a numerical prediction of flow and heat transfer in a welding process. Heat transfer in a baffled channel is calculated in [44N]. A numerical study of combustion of a liquid droplet is given in [43N]. Reference [42N] describes a simulation of premixed flames. Numerical techniques are applied to the creeping flow of a Bingham plastic [41N]. The flow in an impulsively started driven cavity is analyzed in [40N]. Boundary fitted coordinates are used for the calculation of flow in ducts with irregular cross sections [39N]. The flow during the collision of a liquid droplet on a substrate is calculated in [51N]. Finite element modeling is used for the simulation of laser welding [50N]. Particle methods are employed for the numerical solution of the Boltzmann equation [38N].

### 17. Transport properties

#### 17.1. Transport properties

Contributions in this section range from the basic i.e. the influence of low-energy molecular collisions involving a light collision partner (H<sub>2</sub>) upon the transport properties of air to a concern with the transport coefficients for specific systems: textile fibers, common building materials, food products and Seebeck effect materials [1P–5P].

#### 17.2. Thermal conductivity and thermal diffusivity

Strikingly different experimental techniques are used to measure thermal properties of diverse systems. The accuracy of thermal conductivity and diffusivity measurements by the parallel wire method is assessed by a model accounting for the probe radius and contact resistance between material and probe [11P]. A laser-induced grating technique determines the diffusivity of aqueous solutions of methanol [18P]. A transient spherical source method measures the thermal conductivity of liquids and gels [12P]. An AC-heated strip (wire) technique obtains thermal properties of ammonium salts in solid and molten states (thiocyanate, formate, acetate, nitrate) [14P]. Using an apparatus based on the flash method, thermal properties for polycrystalline HgS and Sb<sub>2</sub>S<sub>3</sub> were observed [9P].

A number of papers focus on specific systems using temperature measurements in the system and effective thermal conductivity to express findings. Thus the influence of firing temperature and porosity on thermal conductivity and diffusivity of iron ore pellets are

reported [16P]; the effective thermal conductivity of loose particulate systems measured (273–900 K) [6P]; and the findings of a geothermal project in Albania for rock sample thermal conductivity and temperature profiles in selected boreholes of a region [8P].

Other studies consider: the quantities affecting the thermal conductivity of a magnetic fluid [17P]; polishing and honing abrasive and the internal heat transfer process [10P]; polarization and anomalous heat transport in a ferroelectric (MAPCB crystal) [15P] and thermal effects in a high-performance reactor [13P]. A method of determining temperature variable properties of composite materials is validated by comparison with experiment in [7P].

### 17.3. Diffusion, surface tension, viscosity and radiation properties

The diffusion phenomenon is examined for the very hot electron gas [21P], metal system and semiconductors [19P], and its basic transport expression shown to follow the path of J. Stefan (1871) [24P]. The surface tension of aqueous solutions of lithium bromide containing 1-octanol (simulating heat-pump working fluids) is measured for the first time [20P]. The non-Newtonian behavior of glass melts is considered and four different expressions for representing the gross viscosity effect assessed [25P]. For radiation, properties of cellular ceramics at high temperatures (1200–1400 K) are measured and models are assessed for determining absorptivities for absorbing, emitting and scattering media [22P,23P].

### 17.4. Thermodynamics

Work here clusters about two themes. The first is the extension and refinement of thermodynamic analysis to include evolving interfaces far from equilibrium [26P], work, heat and material exchange between a discrete system and its environment as derived by field-theoretical methods [27P], transport process theory in semiconductors as viewed by equilibrium and irreversible thermodynamics [29P], the reproduction of linear nonequilibrium thermodynamics within the framework of general relativity for static space-times [31P], and perturbational thermodynamics for coupled electrochemical heat and mass transfer [32P]. The second theme is the optimum performance of models of practical systems: optimum operation of irreversible Carnot heat engines of finite size at maximum power output [28P], optimizing the energy output for an endoreversible Carnot refrigerator [33P], and second law analysis of adsorption cycles with thermal regeneration [30P]. Thermodynamic properties for binary mixtures of R-

32/125 are reported based on the Van Der Waals equation of state [34P].

## 18. Heat transfer applications: heat exchangers and heat pipes

Reported work includes the analysis and experimental test of applications conventional and innovational, utilizing materials and designs which extend and enhance heat transfer performance.

### 18.1. Heat exchangers

Numerical analysis is employed to determine the performance of perforated plate matrix exchangers, the heat transfer coefficients in a gas fluidized bed and cross-flow heat exchangers [36Q,21Q,35Q,6Q,26Q,38Q]. Heat exchanger networks are modeled for minimum area and total annual cost and for optimal retrofit. Transient operation is considered for a matrix solar air heater and a shell and tube exchanger [16Q,7Q,3Q,11Q]. A number of sharply focused studies investigate: The heat transfer of elastic, nonNewtonian fluids in rectangular ducts, gas (CO<sub>2</sub>) absorption with wetted flow surfaces, a microporous heat sink for cooling radar systems and exchanger performance in geothermal heating systems [14Q,27Q,24Q,22Q].

Experimental works focus on fluid-to-particle heat transfer under a variety of conditions, low-temperature, helium heat exchangers, and heat exchange in the presence of phase change [4Q,17Q,28Q,32Q,9Q,40Q,20Q,10Q,19Q,18Q]. Yet others report data for exchangers with helical baffles, perforated-plates, propeller driven fluid rotation in double-pipe design, and in conjunction with hot water storage [23Q,31Q,39Q,13Q]. A group of papers provide a general approach and overview of heat exchangers with specific consideration of fundamentals, compact designs, exchanger networks, cost minimization, high-altitude aircraft exchangers, shell-and-tube optimization and trouble shooting, chemical accumulators and the comparative virtues of plate and tubular exchangers [5Q,33Q,37Q,30Q,8Q,12Q,15Q,29Q,2Q,34Q,25Q,1Q].

### 18.2. Design/materials

The use of aluminum is the common thread linking a number of efforts: Micro heat exchangers using porous layers, brazed shell-and-tube for use with noncorrosive gases and liquids, and automotive exchangers [42Q,55Q,64Q,45Q]. The concern with materials continues with the study of plastic crossflow exchangers for the air–water vapor mixtures, fluoropolymer resins for low cost, high performance exchanger material, the



heat transfer behavior between PVC and steel and the electronic packages and semiconductor laser diode array [44Q,63Q,47Q,43Q,57Q].

A significant cluster of works feature phase change as the chief heat transfer design element. The wettability of aluminum plates in an air-to-air heat is evaluated experimentally; the capillary pump loop with phase change is tested for possible use as a space thermal control system; the torque tube heat exchanger for super-conducting generators is analyzed, and the thermal-hydraulic performance for helium-cooled divertors used in large tokamak is optimized [61Q,53Q,58Q,50Q]. Other papers feature bayonet-tube evaporators and condensers in refrigeration practice, a comparison between two approaches to condenser design, a design model for an absorption heat pump rectifier, powerplant generator air-cooler design and exchanger test for structural integrity [54Q,62Q,52Q,46Q,51Q,48Q]. A final group of papers in this area provide general information on heat exchangers, the pinch analysis method including energy factors and exchanger optimization using second law analysis [56Q,59Q,60Q,49Q,41Q].

### 18.3. Direct contact exchangers/cooling towers

These devices are central in water conservation efforts but also occur in electronic component cooling and air purification activities among others. The cross-flow cooling tower, dominant in process, industrial, and power plant applications for half a century has been joined by a growing number of industrial counterflow towers. Mathematical modeling and computer simulation, and cross to counter-flow repack highlight this emerging application [74Q,68Q,75Q,73Q]. For the thermal design of wet, counterflow and crossflow types of mechanical and natural draught cooling towers a detailed, step by step methodology is given using logical decisions, empirical relations and assumptions. Such efforts in cooling tower design and water treatment have overcome many of the difficulties associated with cooling tower use [71Q,72Q,66Q,76Q,69Q]. Cooling tower efficiency and its relationship to energy conservation and overall building or plant efficiency is described [70Q,65Q], and field tests of heat and mass exchangers with steam-gas mixtures presented [67Q].

### 18.4. Enhancement

Attempts to enhance heat transfer rest on strikingly different approaches: The use of porous coatings and inserts; surface modification and surfactants; additives, including solid particle suspensions; twisted tape inserts, vortex generators; spiral coils of finned tubes; and spine finning of tubes [97Q–

100Q,84Q,90Q,92Q,104Q,77Q,102Q,103Q,79Q]. Also considered are compact and miniature exchangers, the effect of flow character (natural, forced and mixed convection) on heat transfer, and the limited influence of a radiating fin array [87Q,80Q,91Q,89Q,88Q]. Several papers report data for free convection and radiation in horizontal finned tube bundles, three-dimensional plate-fin and tube exchangers, preformed trapezoidal fins for tube-in-fin exchangers effective in low Reynolds number flow, and absorption exchanger performance [96Q,85Q,86Q,81Q,83Q]. A final group of works provide general background information regarding heat transfer enhancement [82Q,94Q,93Q,95Q,101Q,78Q].

### 18.5. Fouling/deposits/surface effects

For heat exchangers subject to fouling, investigations focus on the fouling mechanism as well as maintenance strategies and fouling assessments [118Q,115Q,106Q,105Q]. Fine particle deposition in compact plate fin exchangers is studied, the thermal resistance in nonuniform fouling of cross-flow exchanger tubes is analyzed, and progress with gas-side fouling of surfaces reviewed [112Q,114Q,111Q,113Q]. Fireside fouling by ash, slag and corrosion is the focus of several papers [108Q,117Q,109Q]; several others center on scale formation and microbiological growth on the water side and leak detection [110Q,107Q,119Q,116Q].

### 18.6. Reactors — chemical/nuclear

Interest here is directed toward flame support layer geometry and materials on the efficiency of gas radiant burners, the estimation of kinetic and heat transfer parameters for a wall-cooled fixed-bed reactor and the observation of heat transfer in a circulating fluidized-bed combustor [122Q,120Q,121Q].

### 18.7. Thermosyphons — heat pipes

As understanding and the range of application increases these devices continue to interest investigators and designers. The grooved or finned heat-pipe of disk shape is considered for cooling electronic components as well as other applications [142Q,132Q,141Q,131Q,133Q,128Q]. Additional studies consider pressure and velocity effects for the flat-plate design [129Q,134Q], and the influence of working fluids, container materials, and wick structures on the heat transfer, characterized as effective thermal conductivity of the device [123Q]. Specific consideration is given to the stainless steel/ammonia loop, a model to analyze a liquid-metal heat-pipe start up, the development of a heat-pipe thermal diode, vibration effects on the capillary limit for a copper/water design and transient

behavior of the device [140Q,139Q,137Q,130Q,125Q]. The state of our knowledge of the heat-pipe is provided by two papers. One describes the measure of heat transfer performance of an industry standard, wavy plate fin-tube condenser and compares the results with a R22 thermosyphon test rig, analysis revealing excessive fin-tube resistance in the industry standard. Sectioning and microscopic examination confirmed this finding [127Q]. The second describes the use of a double-heat pipe (concentric) to create a large area black body for generating precise spectral irradiance in the red and near-infrared range [138Q]. The device's versatility is further confirmed by its applications in diverse situations: cooling of metal oxide semiconductor thyristors by miniature heat pipes, geothermal use, reciprocating heat pipes under development for engine pistons, and air conditioning in industrial plants [124Q,136Q,135Q,126Q].

#### *18.8. Miscellaneous — thermodynamic analysis/energy conservation/ storage*

For condensers, conditions causing pinch points are identified when using zeotropic refrigerant mixtures, methods for calculating shell-side condensation in rod-baffle configurations and the performance of water and air cooled units predicted [157Q,155Q,154Q]. Waste heat recovery is considered for industrial refrigeration plants, metal-hydride heat transformers and waste-to-energy power plants [156Q,149Q,151Q]. A number of analytical studies examine the performance of energy storage concepts [147Q,158Q,153Q,152Q]. A novel conservation concept is applied to turbomachinery analysis, and the performance of irreversible refrigerators, heat pumps, and thermodynamic water pump examined [145Q,143Q,144Q]. A new graphical technique is presented for assessing the integration of utility systems; a work exchanger network is proposed analogous to the existing heat and mass exchanger networks, and a radiator system presented as an alternative to traditional air conditioning [150Q,148Q,146Q].

### **19. Heat transfer applications: general**

#### *19.1. Aeronautics*

A study of the cooling of aerospace planes at the stagnation point, leading edges of wings, and engine parts by various gases finds hydrogen as the clear winner [1S]. A new model for the prediction of recombination rates of O and N atoms at silica reentry protection systems is based on realistic surface potentials [5S]. All 4 space shuttle orbiters were instrumented for measurement of heat transfer rates and the

results are now compared with previous measurements and analysis [2S]. The fibers in ceramic composites have to be coated to obtain adhesion in reinforced ceramic composites. This was studied in a reaction chamber [3S]. Bolted joints cannot be recommended in satellites [4S]. The design of the cooling system for a lunar base recommends a Rankine cycle for the heat pump [6S]. A thermally controlled test chamber is based on the principle to convect the heat by a layer of cool air away from the chamber [7S].

#### *19.2. Bioengineering*

The microvascular system of a tissue is modeled by a quasisporous medium in an equivalent tube. From experimental results it is concluded that venovenous perfusion can predictably induce hyperthermia [18S]. An inverse method is used to optimize heating conditions in RF-capacitive hyperthermia [17S].

Water transport in meat was studied in an oven at 175C showing that water moves initially toward the center but reverses its direction when the center has reached about 70C [16S]. The heating process in laser heating induced thrombosis of microvessels was predicted by a simple heat transfer model [14S], also the temperature drop and weight loss during meat chilling [8S]. Theoretical and experimental aspects of freeze drying of dairy biomaterials are discussed [13S]. An analysis of freeze drying is based on a model considering a uniformly retreating ice front in a body of spherical geometry [11S]. A model for the study of heat transfer in tissues is developed and tested using a counter-current network [9S]. A new algorithm for identifying the temperature and space dependent conductivity, blood perfusion rate, metabolic rate, and thermal diffusibility is proposed and tested [10S].

A new technique for the production of high purity polymers for biomedical purposes is developed and tested by experiments [15S]. A mathematical model for the cooking of cocktail shrimp describes the heat transfer and microbial inactivation kinetics in agreement with experimental data [12S].

#### *19.3. Digital data processing/electronics*

The first paper in this section offers an overview of cooling technology of electronic systems, characterizing the fan performance and the systems impedance (pressure drop) in the laminar and turbulent flow regimes [19S]. Heat is removed from the printed circuit board to a cooled metal plate (copper, aluminum, molybdenum or alloy) with channels for liquid or air coolant flow [21S]. Attempts to predict the temperature and stress field are made difficult by the involved geometry and length and time scales occurring [22S]. Graphite

fiber reinforced aluminum and copper are considered for module frames providing support and heat sinks. The thermal conductivities are measured [20S].

#### 19.4. Energy

A new model for predicting heat transfer in the rotary combustion engine was formulated [33S]. Combustion technology for gas turbines is reviewed [27S]. A calculation method addresses the temperature distribution in turbine blades [29S]. Heat transfer measurements are reported for endwalls and guide vanes of turbine blades [37S]. Recent modeling of low emission gas turbine combustors includes finite rate chemistry and turbulence [28S].

The radiant efficiency of 4 gas burners was evaluated based on spectral radiosity measurements [38S].

A model based on conservation equations serves to evaluate the effectiveness of dry-cooling systems [26S].

A paper reviews implementation of combined heat and power systems [34S]. The pressure response of a water wall containment cooling system was evaluated experimentally [31S]. A new system of this type is described [30S]. The boiloff pattern in the high pressure core was observed following a small break loss of coolant accident [35S]. The operation of an isolation condenser submerged in a large water pool was observed and evaluated [32S].

The pressure rise and boiling process of the thermo-fluid ITER in a Tokamak plant during a transient accident is studied experimentally [39S]. The screw tube is compared in its action with the swirl tube for the cooling of experimental fusion machines [23S].

The oil heating requirements of floating storage vessels for crude oil are studied [25S]. Phase change thermal energy storage using spherical capsules is studied for refrigeration and air conditioning [24S]. Experimental research studied a 5 mm diameter coaxial pulse tube made of nylon used for a refrigerator [40S].

The thermal resistance of a ball bearing and heat transfer by conduction, convection and radiation is analyzed by computation [36S].

#### 19.5. Environment

The LEK diagram is described as a means to predict overall heat transfer coefficients for building envelopes [45S]. Composite absorbents have better heat transfer characteristics than granular packed beds for heat pump applications [46S]. Thermal testing results are reported for fiber-reinforced plastic building envelopes [41S]. Several correlations describing convection heat transfer for interpane window cavities are examined and their backgrounds discussed [51S]. Experiments studied the insulating behavior of layers of textiles

under wind assault [42S]. Overall heat transfer coefficients of existing wall systems in Turkey were measured. It was found that insulation of the external wall would reduce heating demand by fifty percent [43S]. Plate heat transfer technology can handle all hot fluid demands of hotels and prisons [50S].

The use of the ground as heat source for heat pumps was studied by computer simulation [44S]. The thermal environment of a wellbore is required for a thermal wellbore analysis [48S]. Available software and publications for ground source heating, ventilation and air conditioning are discussed [47S].

Artificial circulation of water can influence average lake temperature [49S]. Environmentally friendly polymer additives to halogenated flame retardants are explored [52S].

#### 19.6. Manufacturing

A large number of papers was again published on castings. Programs for development of models [77S] for continuing casting, strain analysis [56S], mold powders [53S, 54S], simulations of solidification [65S], surface crack formation [79S,80S], process time reduction [66S], cooling [55S], thin strip casting [67S], steel flow and heat transfer [73S] are available.

Three inverse methods estimate heat flux and convection distribution in a work piece subjected to grinding [62S,63S]. Partitioning of heat between two sliding bodies determines grinding process [74S]. Critical factors for thermal damage [75S] are compared for the cutting process [76S].

Analysis considers conditions for metal weld cracking [61S] as well as micropore formation in spray deposition [59S]. The cooling process is investigated for strip cooling [64S] for castings [72S] and for clinkers [58S].

Finite element analysis is applied to machining [68S,70S].

Heat transfer and fluid flow are studied for extruder processing of polymers [57S], for microwave heating of polymers [69S]. The thermal conductivity and contact conductance have been measured in the range 10°C–100°C [71S].

The heat effect in sorption of organic vapors in rubbery polymers is studied experimentally and analytically [78S]. A new technique studies nonisothermal crystallization of polymers at high cooling rates [60S].

#### 19.7. Processing

The study of the heat transfer processes by computer analysis or experiments is extended to more and more manufacturing processes.

A new method is proposed for calorimetry of stirred

tank reactors [105S]. Thermophoretic vapor deposition [106S], injection molding [96S], dendritic growth in solidification [86S], and heat transfer in flowing polymers [94S] were studied. Thermophoresis can decrease particle transfer in a laminar boundary layer by two orders of magnitude [83S]. Russian developed aerodynamic furnaces [104S], process safety [88S] are discussed. Calculations of flame impingement heat transfer are compared with experiments [81S]. Laser heating of engineering materials [107S,108S] and of particles [99S] found attention. Platelet growth is a desirable means for crystal growth [98S,91S]. Simple models can describe the process in furnaces [103S] and rotary kilns [82S]. Experiments carried out at the International Flame Research Foundation [95S] clarified the effect of fuel/air mixing on Nox reduction. Heat transfer was studied in strip rolling [100S], in rotating roll [84S], and in a cement rotary kiln [87S]. Theory and experiments clarify heat transfer at thermoplastic sheet formation [93S].

The drying process is optimized for batch dryers [90S]. The temperature distribution is estimated based on experiments in sterilization and cooling of canned products [85S]. A polypropylene particle was suspended in a high temperature oil bath to measure the overall heat transfer coefficient with end-over-end rotation [102S]. Heat transfer and thermal stress formation are formulated for continuous quenching of aluminum plates [101S]. Drying-induced stress is reviewed for elastic, viscous, and viscoelastic materials [89S]. Effects of variable properties and viscous dissipation is considered for optical fiber drawing of fused silica [92S]. The heat load in a mine ventilation network is simulated for various geothermal parameters [97S].

## 20. Solar energy

Reviewed papers include research on solar thermal technologies, resource assessment and use of renewable energy and energy conservation in buildings. Papers that do not address heat transfer issues, for example, papers dealing specifically with photovoltaics or wind energy, are not included.

### 20.1. Radiation characteristics and related effects

The majority of the published research concerns methods to improve predictions of solar radiation. Interpretation of satellite images are discussed by [2T,4T]. Models include a statistical regression to predict daily radiation in locations or during periods of time for which measured data are not available [1T], a physically based model of the radiative balance over

snow [3T], use of monthly average values to predict hourly values [8T], and a new algorithm to determine the integral Rayleigh optical thickness [5T]. A comparison of models of diffuse radiation for prediction of total radiation on tilted surfaces is presented by [9T]. Site specific data are an inventory of heat fluxes from residential and industrial sections of Lodz, Poland [6T]. A new optical method to measure directional spectral emissivity and surface temperature is used in a high flux solar furnace [7T].

### 20.2. Nonconcentrating collectors

The maturity of the field of nonconcentrating solar collectors has resulted in a continuing decrease in the number of papers on this topic. Analytical studies address solar gain and heat storage characteristics of a collector constructed of soil/sand/concrete [10T], comparison of predicted and measured gas conduction in an evacuated tube solar collector [11T], optimization of flat-plate air collectors [12T], characterization of natural convection in a corrugated enclosure [13T], and a model for estimating the thermal resistance of the absorber/coolant in systems using advanced heat transfer mediums [14T]. Experimental data are presented for a pentane-based collector intended for solar thermal water pumping [15T]. Measurements of storage tank temperature are used to estimate collector optical and heat loss characteristics for a water heating system [16T].

### 20.3. Concentrating collectors and systems

The topics considered are divided into two categories: concentrator/reflectors and receivers. In the area of concentrators, [22T] presents experimental data showing that a solar concentration of 50,000 is possible with a dielectric, nonimaging concentrator. A two stage concentrator with on-axis tracking intended for use with high efficiency solar cells achieves concentrations as high as 300 [17T]. [26T] describes a focusing concentrator that uses two reflecting troughs. He compares performance of this design to that of conventional parabolic troughs. [21T] shows how tailored edge-ray concentrators in two-stage solar collectors can be constructed using a simple method of strings. Modeling of thermal and optical behavior of line-axis concentrating collectors is discussed in terms of modifications in geometry [19T]. Surface characterization of parabolic reflecting surfaces using close range photogrammetry is demonstrated [27T].

Work on receivers addresses the suitability of modeling arrays as a homogeneous medium [25T], refinement of an analytical technique for the prediction of flux distribution on receiver surfaces [20T], modeling of

flow in volumetric receivers [24T], heat transfer through gases at low pressures [18T], and analysis of radiation and conduction through honeycomb-cored panels for use in a space based power system [23T].

#### 20.4. Buildings

Energy conservation in buildings continues to attract significant research on materials and simulation models. Papers that relate primarily to fenestration include design charts for appropriate selection of multiple glazed windows in terms of thermal, sound, daylight and solar transmission [43T], models of solar heat gain in windows with a venetian blind inside double glazing [39T,40T], effect of glazing shape on energy consumption in a commercial building [38T], and modeling of solar gain through windows for three sites in Jordan [46T].

Studies associated with the building envelope include modeling of radiation and conduction across transparent honeycomb insulation [29T], development of simple algorithms to predict energy savings of transparent insulation [35T], an experimental study to evaluate the impact of various radiant barrier systems on cooling loads [28T], experimental characterization of energy consumption due to infiltration [32T], use of the overall transfer value to predict heat gain through external walls and roofs of large buildings [30T], a review of the interaction between environment and damage of concrete [44T], and transient modeling of vertical temperature distributions in an atrium [47T]. More applied studies are experimental comparison of five protected membrane roofs installed between 1981 and 1992 [36T], simulation of heat exchange through structural panels commonly used in refrigerating storage [34T], a model of the heat transfer from cattle useful for the design of livestock buildings [33T], determination of heat demand in public baths [49T], assessment of occupancy patterns on solar heating contribution of roof space solar energy collectors [41T], discussion of use of the roof as a solar collector [45T,48T], comparison of three thermal simulation programs) ESP, HTB2 and SERIRES) for a range of passive designs used in the UK. [42T], and minimization of heating and ventilation costs in greenhouses [37T]. [31T] assess the impact of using different weather files on building energy use predicted by BLAST.

#### 20.5. Water and space heating

Characterization of the effect of various off-peak and water use schedules on thermal efficiency of electric water heaters is intended to allow comparison of water heating technologies (including solar) for reduction of peak electrical demand [52T]. [51T] com-

pare use of various renewable sources for integration with residential heat pumps in Poland. [50T] models heat transfer from finned surfaces in a thermal storage tank.

#### 20.6. Cooling and refrigeration

[53T] presents an analytical solution for the effect of air on heat and mass transfer rates during absorption of water vapor from a film of lithium bromide flowing down a vertical wall. The heat exchangers in 20-ton lithium bromide/water absorption cooling system were optimized in terms of system cost [56T]. In related papers, the effects of various operating and design parameters on solar fraction are modeled [57T,58T].

Thermodynamic optimization of solar-driven refrigerators is presented by [55T]. Limited experimental data on a carbon-ammonia refrigerator driven by a thermosyphon heat pipe are presented along with plans to develop a solar ice maker [54T].

#### 20.7. Storage

Papers that address the use of storage as part of a system are discussed by application in the appropriate section. See, for example papers [84T,89T,92T] in the section on power generation, and Ref. [50T] in the water and space heating section.

[59T] suggests that exergy efficiency is the most appropriate value to determine storage efficiency. The paper evaluates variable and constant temperature systems. [62T] examines entropy production in a cylindrical sensible heat storage system. [60T] considers irreversibilities of a latent heat storage module with a cylindrical shell surrounding a coaxial tube. A two-dimensional model of melting in a rectangular enclosure heated from one side shows heat transfer is dominated by convection [61T]. [63T]'s numerical model of latent heat storage placed in the ground indicates that thermal performance is dominated by thermal diffusivity of the phase-change material. [64T] predicts the performance of a thermal storage system in which pipes with brine flowing inside are sequentially charged and discharged. The model focuses on the formation of ice and liquid on the outside of the pipes.

#### 20.8. Stills and desalination

A new desalination process that dehumidifies air by pervaporation through hydrophilic or microporous hydrophobic hollow fibers and then dehumidifies with cooling water is investigated in a 6 liter/hour pilot plant. Solar energy is suggested as one possible heat

source for the hot water that passes through the hollow fibers in the recycled air-sweep pervaporation process [65T].

The majority of papers on solar stills present models to predict effects of various design parameters on performance of traditional designs. [66T] considers the effect of evaporation area on distillation yield. Analysis of the effects of inlet water temperature and flow rate on heat and mass transfer is presented by [67T]. A series of papers model the effects of glass cover inclination [68T,71T], water flow rate over the glass cover [72T], and collector area in a system with a collector and heat exchanger [70T]. Comparison of temperatures and heat and mass transfer rates in solar stills and solar evaporators shows that evaporation in stills is much less than that in open evaporation [69T]. [73T] considers coating the transparent cover plate with  $\text{SnO}_2$ . [74T] applies a simple empirical model to show the suitability of using solar stills to provide drinking water in Iran.

#### 20.9. Ponds

A one-dimensional model of a closed-cycle salt gradient pond is used to investigate methods of salt cycling. Results indicate seasonal surface flushing is the most desirable [75T]. Models of mixing and entrainment due to an injecting diffuser are presented to analyze a new gradient maintenance technique for salt-gradient ponds [76T]. Stability analysis of layers with adverse temperature gradients is used to model ponds where the salt concentration gradients is intended to prevent convective mixing induced by absorption of solar radiation [77T]. Enhancement of storage in the ground beneath solar ponds predicts as much as a 36% reduction in salt requirement [78T]. [79T] presents field tests of a nonsalt pond for greenhouse heating.

#### 20.10. Cooking and drying

The two papers in this study present preliminary test data for a prototype V-groove back-pass solar air collector intended for drying [81T] and a coconut oil flat-plate collector for solar cooking [80T].

#### 20.11. Solar chemistry

[82T] present experimental data of demonstration of photocatalytic oxidation with titanium dioxide of wastewater from 5-fluorouracil manufacturing. The addition of hydrogen peroxide increased reaction rates. At UV intensities as low as  $15 \text{ W/m}^2$  decolorization rate remained high. Destruction of organic compounds in water was studied using titanium dioxide supported

on silica gel. Both model and experiments are presented [83T].

#### 20.12. Power generation and industrial applications

This diverse group of papers address sensible heat storage in conjunction with dish-Stirling systems [89T], thermoelectric generation [85T], direct steam generation in parabolic trough power plants [88T], combined power generation and desalination in an OTEC plant [91T], use of seawater as the working fluid in a regenerative-reheat cycle [90T], Kalina absorption power cycles [86T], metal hydride hydrogen storage in hydrogen energy systems [92T], control of solar process heat plants [87T], and heat storage of magnesium nickel hydride used for recovering waste heat [84T].

### 21. Plasma heat transfer and magnetohydrodynamics

#### 21.1. Plasma characterization

A thermodynamic description of an atmospheric pressure nonequilibrium plasma in supersonic nozzle flow is presented by Chen and Eddy [1U]. Thermodynamic relations are extended to include deviations from composition equilibrium without going through a full scale chemical kinetics calculation, and the results are presented in the form of multi-dimensional graphs. The influence of tungsten vapor on the thermodynamic and transport properties of an SF<sub>6</sub> plasma is presented by Chervy [2U] in the form of results of property calculations, and the conclusion is reached that below a molar concentration of 10% only the electrical conductivity is affected. Tsintsadze et al. [9U] present a theory of a plasma in equilibrium with a blackbody radiation field. The interaction of an electric arc with a transverse magnetic field is described by Speckhofer and Schmidt [8U] using experimental and theoretical results, including a time dependent simulation of arc instabilities at large magnetic fields. A description of a microwave generated nonequilibrium hydrogen plasma uses a three-temperature thermochemical model, and this model is applied to a diamond deposition reactor [7U]. Several studies concern themselves with description of plasmas in arcjet thruster configurations. Megli et al. [3U] use a two-temperature model with the composition calculated with a chemical kinetics approach, with the results demonstrating the expected strong deviations from equilibrium for the case of a N<sub>2</sub>/H<sub>2</sub> arcjet. A similar calculation is presented for a hydrogen arcjet in [5U] with a somewhat different numerical approach. The erosion of the cathode of a magnetoplasma dynamic thruster has been modeled using a

finite element algorithm [4U]. An experimental study using mass spectrometry and optical spectroscopy in a low pressure plasma jet has been used to characterize the conditions which are expected during entry into the atmosphere of Mars or Titan [6U]. In a review article, Zhukov proposes a classification method for plasma torches and describes various applications of the torches [10U].

### 21.2. Laser–plasma interaction

A self-consistent model of the absorption profile of an ultrashort laser pulse by a high density plasma is given by Rozmus et al. [12U]. The interaction between a laser pulse and the plasma in front of a solid is simulated by Mazhukin et al. [11U].

### 21.3. Applications

A number of publications deal with describing plasmas under conditions and in configurations for specific applications. The plasma heating of a tundish is simulated by modeling a steam jet impinging on water [13U]. The problem of increasing the plasma generator power in a ladle furnace is addressed by Neuschuetz and Stueber [25U], and the result shows that addition of up to 40% CO<sub>2</sub> to the argon as plasma gas will significantly increase power dissipation and heating rate while adding only an insignificant amount of oxygen take-up by the metal. Two papers deal with plasma cutting issues, one describing a model for the heat flux distribution in the work piece [21U], the other modeling the movement of the liquid metal inside the cut, indicating a reduced heat transfer rate after formation of the liquid metal layer [24U]. Two papers deal with arc welding, one describing results of a simulation of the heat transfer and fluid flow for different arc currents, electrode geometries and arc lengths [16U], the other showing results for a new method of underwater welding using gas shielding to reduce the arc pressure [15U].

Three papers are concerned with the plasma–particle interaction in plasma spray applications, two describing the particle heating and trajectories in d.c. spray jets [27U,19U], and the third one analyzing the heat transfer and fluid flow in a d.c.–r.f. hybrid reactor [23U]. Plasma treatment of titanium carbide powders is described in two publications by the same group of authors, one presenting a study of the influence of the particle injection on the r.f. plasma [29U], the other concentrating on the evaluation of the morphology and composition of the powders in the experiments [18U]. Synthesis of WC-Co powders in an argon-hydrogen plasma with acetylene as carbon source is described by Fan et al. [17U], and the need for hydro-

gen for improving the heat transfer and avoiding formation of carbon particulates is pointed out.

Two papers are concerned with the plasma surface hardening process of steel, one using a finite element model for describing the thermal diffusion of the nitrogen in the solid [26U], the other presenting some experimental results to verify the model predictions [20U].

Plasma heat transfer in the processing of microelectronic components is the subject of two papers, one describing the measured temperature rise of a multi-layer structure on a silicon substrate exposed to a low pressure argon-hydrogen plasma [22U], the other presenting a model for wafer heating during etching as a function of ion flux to the surface, helium cooling of the backside, and different wafer clamping arrangements [28U]. A model for the heat dissipation in plasma based ozone generators and its influence on the ozone generation efficiency is presented by Bes et al. [14U].

### 21.4. Magnetohydrodynamics

MHD continues to provide interesting problems for numerical model solutions, although majority of the publications treat applications other than MHD power generation. An analysis of the thermal efficiency of a MHD generator based on optimal power density and including component inefficiencies is given by Sahin et al. [40U]. Several papers deal with the influence of a magnetic field perpendicular to a free convection flow field of an electrically conducting fluid with different configurations: along a semi-infinite vertical plate with radiation heat transfer included [41U], inside a cubic enclosure [39U], from a horizontal cylinder with forced convection included [31U], for the same configuration but with the cylinder inside a porous medium [30U], from a cone and a wedge inside a porous medium [36U], within a shallow porous cavity [34U], and within an inclined rectangular porous cavity [35U]. In general, results are obtained for different boundary conditions and/or for different values of the governing dimensionless parameters, e.g. Hartmann number and Rayleigh number.

Further modeling results include configurations of MHD flow between two infinitely long, insulated parallel plates with one plate moving and the other stationary [32U], and past a continuously moving porous plate with a similarity transformation for investigating the effect of suction or injection, and magnetic field on heat transfer and skin friction [37U]. The effects of a combination of rotation and translation of a rotating disk on the MHD flow of an electrically conducting, compressible viscous fluid are described in [33U]. Hung et al. find that the instabilities in a MHD

flow of a condensate film along a vertical plate with constant heat flux can be reduced by the applied magnetic field [38U].

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